

R&S®ZNA

VECTOR NETWORK ANALYZER

Master the most challenging measurement tasks



Product Brochure
Version 06.00

ROHDE & SCHWARZ
Make ideas real



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AT A GLANCE

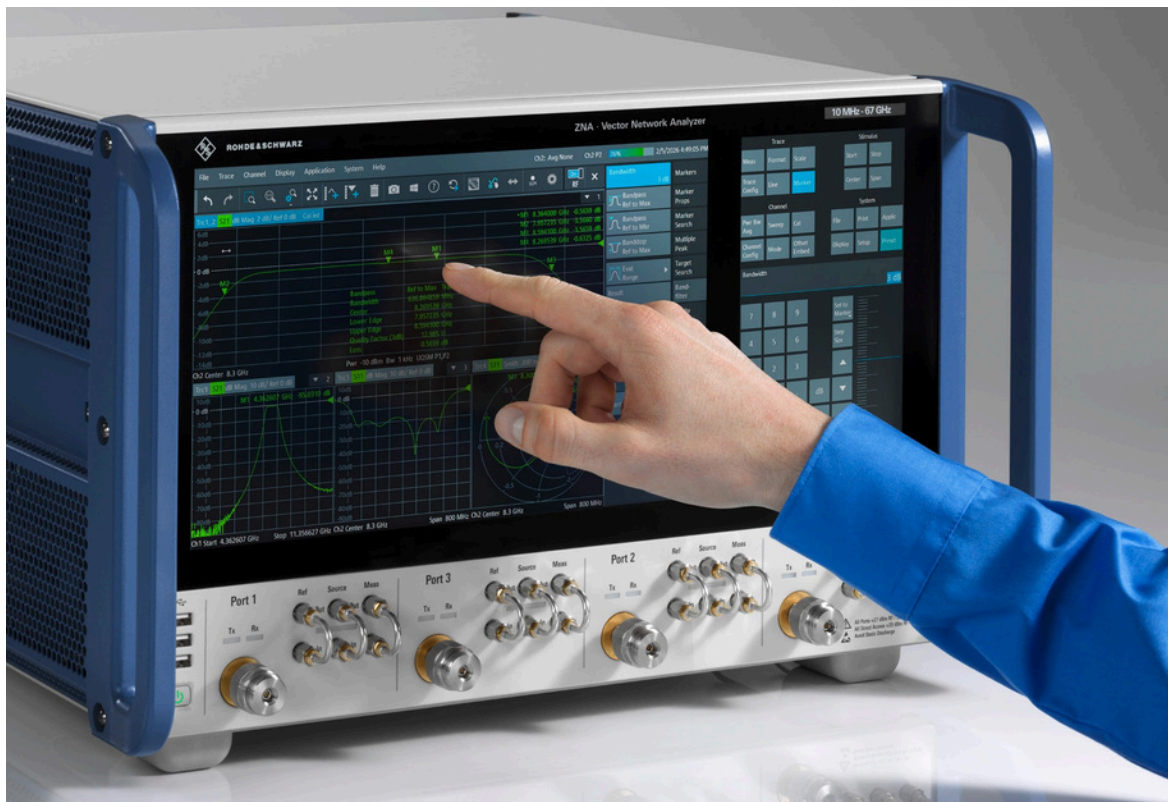
Offering outstanding RF characteristics, a unique and comprehensive hardware architecture and a DUT oriented operation concept, the R&S® ZNA high-end vector network analyzer makes demanding measurements easier than ever before.

The R&S® ZNA features exceptional stability, low trace noise and excellent raw data, making it a perfect choice for development and production applications that require high accuracy, e.g. for developing and producing components and modules for A&D and satellite applications.

The R&S® ZNA offers four internal, phase coherent sources, allowing independent control of the signal's frequency at each port as well as phase measurements on mixers. It provides two internal local oscillator (LO) sources, a true multichannel receiver architecture, pulse generators and modulators, an internal combiner, selectable reference

signal access points, preamplifiers and comprehensive trigger and synchronization capabilities. These hardware features make the R&S® ZNA a universal, compact test system for active and passive device characterization. Even intermodulation measurements on mixers and receivers can be performed without external signal sources, minimizing test time and simplifying test configuration. Thanks to the phase coherent digital sources and receivers, no reference mixers are needed for mixer phase measurements, and test setups are configured just as easily as for non-frequency-converting S-parameter measurements.

Users can operate the R&S® ZNA via two independent touchscreens



The analyzer's DUT-centric operating concept makes it possible to achieve the desired setup at an unrivaled speed. Users can control sophisticated measurements at a glance with dedicated dialogs that show the setup schematics and all of the essential test parameters.

The R&S®ZNA characterizes low-noise amplifiers (LNA), receivers, frequency-converting DUTs and transmit/receive (T/R) modules precisely and efficiently; the DUT needs to be connected only once. The instrument provides numerous software applications, e.g. for intuitive configuration of group delay and spectrum measurements.

Various menu-based calibration procedures are available to help users calibrate even complicated setups efficiently and reliably. All the calibration methods supported by the R&S®ZNA can be expanded using a special calibration technique referred to as R&S®SMARTerCal. This technique combines system error correction with absolute power level correction, minimizing the number of calibration steps even with active DUTs, which involve considerable measurement effort.

R&S®ZNA models

| 100 kHz | 10 MHz | 26.5 GHz | 43.5 GHz | 50 GHz | 67 GHz | 70 GHz | 72 GHz | 110 GHz | 117 GHz |
|--|--|----------|----------|--------|--------|--------|--------|--|---------|
| R&S®ZNA26-B16 direct source and receiver access | R&S®ZNA26 2-port and 4-port, 1, 2 and 4 sources ¹⁾ | | | | | | | | |
| R&S®ZNA43-B16 direct source and receiver access | R&S®ZNA43 2-port and 4-port, 1, 2 and 4 sources ¹⁾ | | | | | | | | |
| R&S®ZNA50-B16 direct source and receiver access | R&S®ZNA50 2-port and 4-port, 1, 2 and 4 sources ¹⁾ | | | | | | | | |
| R&S®ZNA67-B16 direct source and receiver access | R&S®ZNA67 2-port and 4-port, 1, 2 and 4 sources ¹⁾ | | | | | | | R&S®ZNA67EXT Single sweep up to 110 GHz | |

¹⁾ With all models, the internal (second) LO generator is optionally available at the rear panel as third or fifth source respectively (up to 26.5 GHz).

KEY FACTS AND BENEFITS

Four internal phase coherent sources

- ▶ Compact multiple source setups
- ▶ Convenient phase measurements on mixers
- ▶ Phase coherent DUT stimulation and true differential measurements

Two internal LOs

- ▶ Excellent trace noise as low as 0.005 dB (spec.) and 0.002 dB (typ.) at 100 kHz IF bandwidth (IFBW)
- ▶ Fast mixer measurements
- ▶ More accurate phase results due to parallel signal sampling
- ▶ Rear panel LO output for mmWave systems and general purpose applications

Eight truly parallel measurement receivers

- ▶ Measurements on multipath DUTs and antenna arrays, use of analyzer as a powerful core in antenna test systems

Flexible signal routing and path access

- ▶ Internal combiner for intermodulation and embedded LO converter group delay measurements
- ▶ Reference signal access before or after source step attenuator for low trace noise even with very low stimulus signals (e.g. for high gain DUTs)
- ▶ Direct IF access for antenna test systems with external up/down conversion
- ▶ Rear panel LO output and direct IF input for compact mmWave test setups: 2/4-port mmWave converter setups with 2/4-port R&S®ZNA, without additional external source

Four internal pulse modulators

- ▶ Two-tone and bidirectional pulsed signal measurements

Phase measurements on mixers without reference mixers

- ▶ Simple mixer tests in a compact setup

Noise figure measurement on amplifiers and mixers

- ▶ Internal preamplifier (R&S®ZNAxx-B302/-B312) for low-noise DUTs
- ▶ Quickset configuration dialog for fast and optimized amplifier noise figure measurements

Spectrum analysis option

- ▶ DUT characterization and spurious search without reconnecting the DUT to a spectrum analyzer

Group delay measurements on frequency converters with embedded LOs

- ▶ Reliable, straightforward satellite receiver measurements

High dynamic range

- ▶ Dynamic range of 147 dB (typ.) and up to 170 dB (typ., with options)
- ▶ Characterization of high-rejection filters
- ▶ Short test times and low trace noise

Outstanding receiver sensitivity

- ▶ Noise floor < -120 dBm (spec.)¹⁾
- ▶ Noise level down to -157 dBm (typ., with options)²⁾

Exceptional source and receiver linearity

- ▶ 0.03 dB receiver linearity in the range from -50 dBm to 0 dBm
- ▶ Accurate amplifier testing even at very high and low power levels

Wide power sweep range

- ▶ Power sweep range of 100 dB (typ.)
- ▶ Versatile compression measurements

Low trace noise

- ▶ Trace noise of < 0.001 dB (at 1 kHz IF bandwidth)
- ▶ Accurate, highly reproducible measurements

DUT-centric operating concept

- ▶ Easy startup, short configuration times

Compact instrument, quiet operation

- ▶ Acoustic noise as low as 42 dB(A)
- ▶ Small footprint, low noise pollution

SCPI recorder

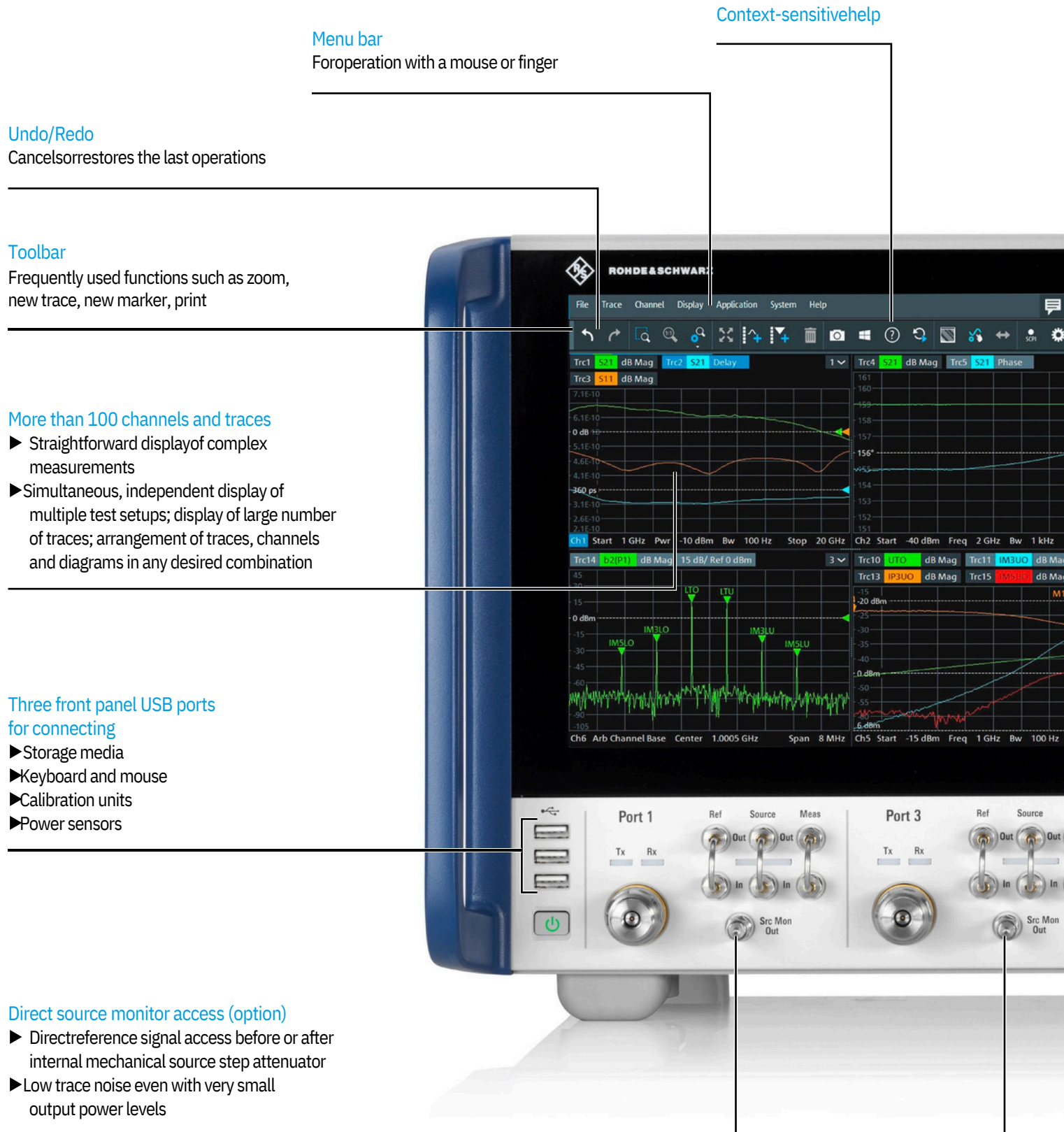
- ▶ Simplifies automated complex measurement setups
- ▶ Standard feature

¹⁾ Specification, without options, at 1 Hz IF bandwidth.

²⁾ Applies for port 2, at 1 Hz IF bandwidth, with R&S®ZNAxx-B16 reversed coupler operation and R&S®ZNAxx-B302 preamplifier options. (xx designates the R&S®ZNA model: R&S®ZNA26, R&S®ZNA43, R&S®ZNA50 and R&S®ZNA67.)



STATE-OF-THE-ART USER INTERFACE



12.1" touchscreen with state-of-the-art graphical user interface (GUI)

Softkeys and soft panel

- ▶ Logically structured menus: everything in view without scroll bar
- ▶ All parameters for a test setup presented in straightforward GUI dialogs
- ▶ Measured traces can be dragged and dropped



Touch panel

Instrument control and display of macros

Soft roll key with locking function

Status LEDs

Calibration status, remote operation, etc.

Direct source and receiver access (option)

Status LEDs for each port indicating

- ▶ TX/RX operation
- ▶ Input active

REAR PANEL CONNECTIONS

Display ports

- ▶ DisplayPort
- ▶ DVI-D

Internal LO signal output (option)

- ▶ LO source for mmWave converter setups (standard internal LO or optional 2nd internal LO)
- ▶ General-purpose, configurable RF source up to 26.5 GHz (optional 2nd internal LO)
- ▶ Up to +25 dBm output power

Trigger board (option)

- ▶ Three additional trigger inputs
- ▶ Four trigger outputs
- ▶ Four connectors for pulse modulator control
- ▶ Ready for trigger (output)
- ▶ Busy (output)
- ▶ RF interlock control (input)

GPIB port

Standard control and sync connectors

- ▶ Reference frequency output: 10 MHz, 100 MHz
- ▶ Reference frequency input: 1 MHz to 50 MHz, 100 MHz, 1 GHz
- ▶ Trigger input

LAN port

SSD (removable)



Four USB ports

- ▶ Storage media
- ▶ Keyboard and mouse
- ▶ Calibration units
- ▶ Power sensors

USB control

For remote device control via USB

Modular design for easy maintenance

Control PC and power supply

Direct control interface (option)

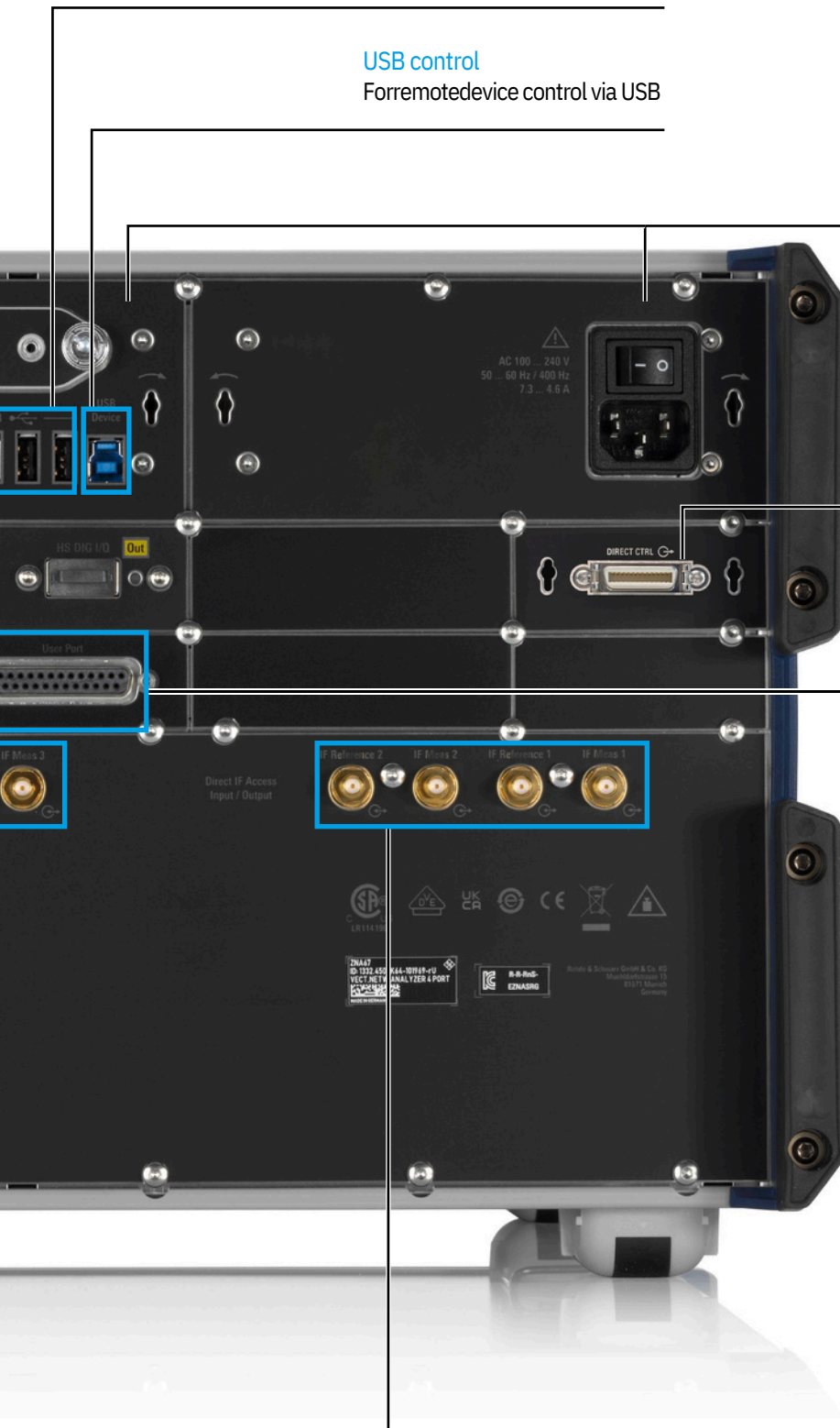
Quick communication with external devices, e.g. control of R&S® ZN-ZCG

User port

- ▶ Digital I/Os
- ▶ Power supply

Direct IF access (option)

- ▶ I/Os (input/output switchable); IF bandwidth, output: 2 GHz
IF bandwidth, input: 1 GHz
- ▶ Access to measurement and reference receiver IF of each port



UNIQUE OPERATING CONCEPT WITH TWO TOUCHSCREENS

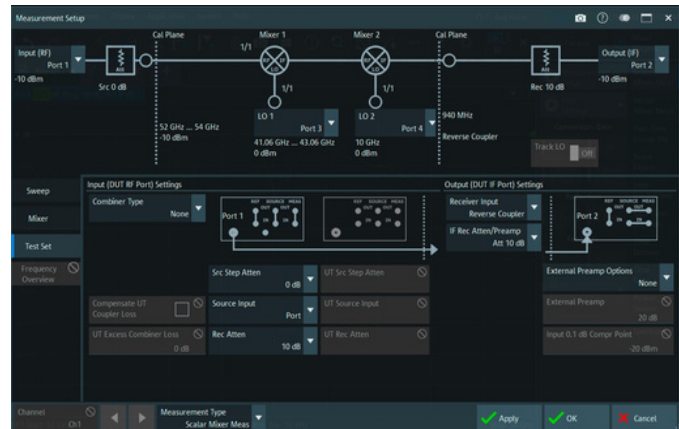
Keep things in perspective with all-in-one GUIs and optimize your setup with single parameter adjustment.

Operation using touch gestures

Users can operate the R&S®ZNA via two independent touchscreens:

- ▶ Innovative control panel on the right instead of mechanical keys which can wear out over time
- ▶ 12.1" touch display on the left for configuring and displaying measurements

The dual-screen operating concept offers utmost flexibility in configuring measurements. Touch gestures are used to zoom, move traces and add markers. Traces, channels and diagrams can be dragged and dropped to arrange them in any desired combination. The control panel on the right can, among other things, be used to display macros, remote control commands and auxiliary tools.



All-in-one dialog for intermodulation measurement on a double converting receiver

Three alternatives to arrive at the desired setup

1. Conventional approach

For general configuration and for basic measurement quantities, such as S-parameters, power and ratios, users can take the conventional approach to configure measurements on the R&S®ZNA. They can select the parameters for a desired setup, e.g. power parameters, the number of points, and the measurement type and measurement quantity.

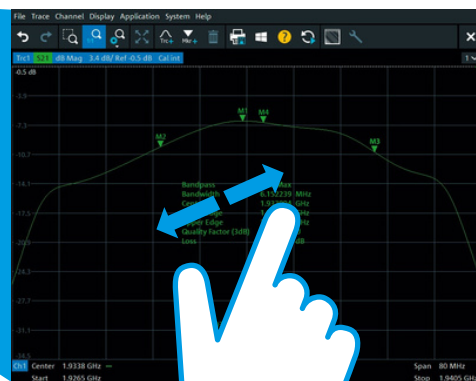
2. All-in-one dialogs—keeping track even of sophisticated setups

For complex setups, such as intermodulation on mixers and noise figure tests, all-in-one dialogs show all of the key parameters otherwise distributed among several menus on a single display. The hardware is configured interactively using graphic elements. Test parameters such as frequencies, power levels and bandwidths are set via pull-down menus and input fields. Users see all relevant information at a glance, not missing a single parameter. Measurement traces for any desired measurement quantities can then be dragged and dropped to any desired position.

Zoom function



Users can zoom with a simple finger gesture or by dragging the mouse. The background color of the screen can be configured as desired.





Control of the R&S®ZNA via touch panel. Users benefit from all-in-one dialogs, which provide a clear overview of all key parameters and help to keep track of the overall measurement configuration.

Trace analysis functions

A wide variety of trace analysis functions provide a clear overview of key parameters:

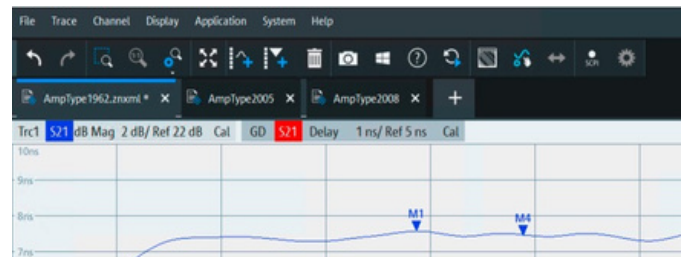
- ▶ Ten markers per trace, including analysis functions and conversion to desired unit
- ▶ Automatic bandwidth measurement on filters
- ▶ Limit and ripple check with configurable pass/fail indication
- ▶ Statistical trace analysis including maximum, minimum, RMS, peak-to-peak and compression point
- ▶ Equation editor for complex trace mathematics

Fast switching between instrument setups

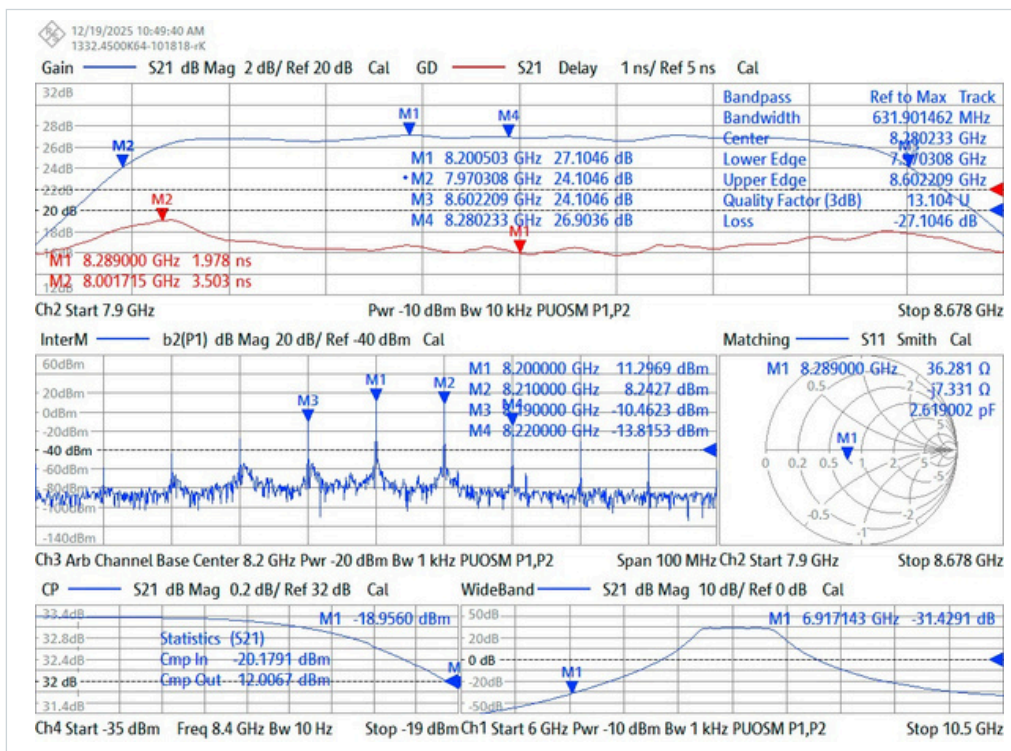
With the R&S®ZNA, multiple setups can be kept in memory simultaneously, allowing users to switch quickly between measurement tasks. This feature is especially advantageous with DUTs that deliver a variety of complex results, as it provides a quick overview and simplifies operation.

3. Step by step to the desired setup: the DUT-centric wizard

Another alternative is a step-by-step, DUT-centric approach. In a first step, the user defines the type of DUT (e.g. mixer) and its key data (e.g. maximum/minimum input power level and frequency ranges). The wizard then prompts the user, in easy-to-follow steps, to define the required settings and measurement parameters, using DUT-specific terms (“Conversion Gain RF to IF” or “Feedthrough LO to IF”). Properly sizing and positioning the display ensures a clear overview, even when there are many result traces.



Setups in the tabs can be switched on with a mouse click.



Properly sizing and positioning the display areas ensures a clear overview even when there are many result traces.



The R&S®ZNA comes with an extensive range of hardware options

TOP-CLASS HARDWARE COMPONENTS

The R&S®ZNA comes with an extensive range of hardware options, allowing customized configuration for the intended use.

4-port model with four internal sources

The R&S®ZNA is available with up to four internal sources (R&S®ZNAxx-B3¹⁾ option, 3rd and 4th internal source for 4-port models). The user benefits from a powerful, compact system that can even perform intermodulation measurements on mixers and receivers with two converter stages. The digitally controlled, phase coherent and phase repeatable sources allow phase measurements on mixers and converters without external reference mixers.

2-port models with two internal sources

Options for second internal RF/LO sources (R&S®ZNAxx-B52), an integrated combiner (R&S®ZNAxx-B212), the rear panel LO output connector (26.5 GHz) and preamplifiers (R&S®ZNAxx-B302/-B312/-B501/-B511) make the R&S®ZNA an extremely compact and effective tool for comprehensive characterization of DUTs with two test ports. Especially the following measurements are supported:

- ▶ Intermodulation on amplifiers
- ▶ Noise figure test
- ▶ Group delay test on (high-gain) embedded LO converters for satellite applications or T/R modules (using R&S®ZNA-K9 two-tone technique)
- ▶ Mixer test (with LO up to 26.5 GHz, rear panel LO out connector)

¹⁾xx designates the R&S®ZNA model (R&S®ZNA26, R&S®ZNA43, R&S®ZNA50 and R&S®ZNA67).

Direct IF access

When used as inputs, the R&S®ZNA-B26 direct IF access ports provide direct access to the internal IF signal paths. The IF frequency is selectable with 1 GHz bandwidth, which provides a high degree of freedom for system integration, especially when integrating the analyzer into antenna test systems with external mixers. When used as outputs, the R&S®ZNA-B26 ports make it possible to record and analyze data using external equipment.

Synchronization and trigger capabilities

The R&S®ZNA offers a comprehensive range of synchronization and trigger features such as diverse trigger inputs and outputs, e.g. for test status indication, definition of criteria for logical decision-making, RF power shutdown, flexible test sequence control in pulsed measurements, synchronization of external devices, and for timing control during test sequences in production. The R&S®ZNA-B91 option (trigger and control I/O board) acts as an interface for the input and output of signals.

Second internal LO source and mmWave converter LO output

The second internal LO source (R&S®ZNA-B5 option for 4-port models, R&S®ZNAxx-B52 second source and second LO option for 2-port models) allows two ports to receive signals at different frequencies. This means that two frequencies can be measured simultaneously, e.g. the RF and the IF signal of a mixer, making the measurement twice as fast and reducing trace noise.

The optional R&S®ZNA-B8 mmWave converter LO output makes the analyzer's internal LO available on the rear panel, e.g. for feeding mmWave converters connected to the R&S®ZNA²⁾. Alternatively, the second LO can be used as a general-purpose RF source, e.g. for external mixers.

(The R&S®ZNA-B8 rear panel LO output is limited to the frequency range from 10 MHz to 26.5 GHz independent from using the standard or optional second internal LO.)

Eight internal pulse generators and four internal pulse modulators

Eight pulse generators and four modulators make it possible to generate pulsed two-tone signals and bidirectional pulsed signals, e.g. for intermodulation measurements on T/R modules. The pulse generators are enabled with any of the following options: R&S®ZNAxx-B4n (internal pulse modulator for port n) and R&S®ZNA-B91 (trigger and control I/O board). The trigger and control I/O board alone enables use of the internal pulse generators to control internal or external pulse modulators (e.g. to generate pulses with a duration of < 40 ns). Point-in-pulse measurements are delivered by the base unit; pulse profile measurements are added with the R&S®ZNA-K7 option.

²⁾ Configuration of the R&S®ZNA-B8 output for use with mmWave converters requires the R&S®ZNA-K8 option (mmWave converter support).

Internal combiner

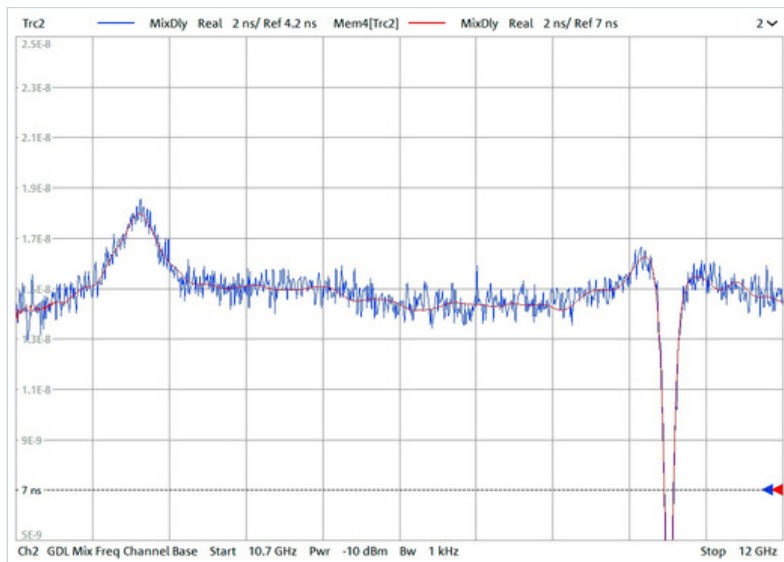
A switchable internal combiner (R&S®ZNAxx-B213 for 4-port models, R&S®ZNAxx-B212 for 2-port models) combines the signals from source 1 and 3 (or a second internal source for 2-port models) to provide a two-tone signal at port 1. This enables intermodulation measurements and embedded LO group delay measurements (with R&S®ZNA-K9 option) to be carried out without additional external equipment.

Direct source and receiver access, source monitor (reference signal) access before or after source step attenuator

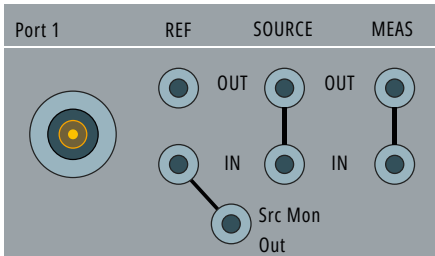
The R&S®ZNAxx-B16 direct source and receiver access option provides direct access to the source and receiver paths. On the one hand, this yields highest sensitivity as the internal coupler can be bypassed, thus avoiding the coupler attenuation, on the other hand, it supports e.g. external high-power test setups. Testing

at low stimulus levels is further improved with the R&S®ZNAxx-B501/-B511 low-power spurious reduction option. An isolation amplifier provides optimized spurious reduction, delivering excellent signal purity for power levels down to -110 dBm and below.

The R&S®ZNAxx-B161 and R&S®ZNAxx-B163 direct source monitor access options make the R&S®ZNA even more versatile. They provide direct access to the reference signal, i.e. they allow the reference signal to be picked up before the internal source step attenuator. With the step attenuator set to high attenuation for very small output power levels, picking up the reference signal before the source step attenuator will provide a reference signal strong enough to deliver low-noise traces, thus providing high accuracy even with high gain DUTs such as satellite and radar modules.



Group delay measurement on a 60 dB gain embedded LO converter (IFBW = 10 kHz for both measurements, shown as blue and red traces). Blue trace: poor trace noise with the low-level reference signal picked up after the source step attenuator. Red trace: minimized trace noise with the reference signal picked up before the source step attenuator, yielding a high signal-to-noise ratio (SNR) at the reference receiver.



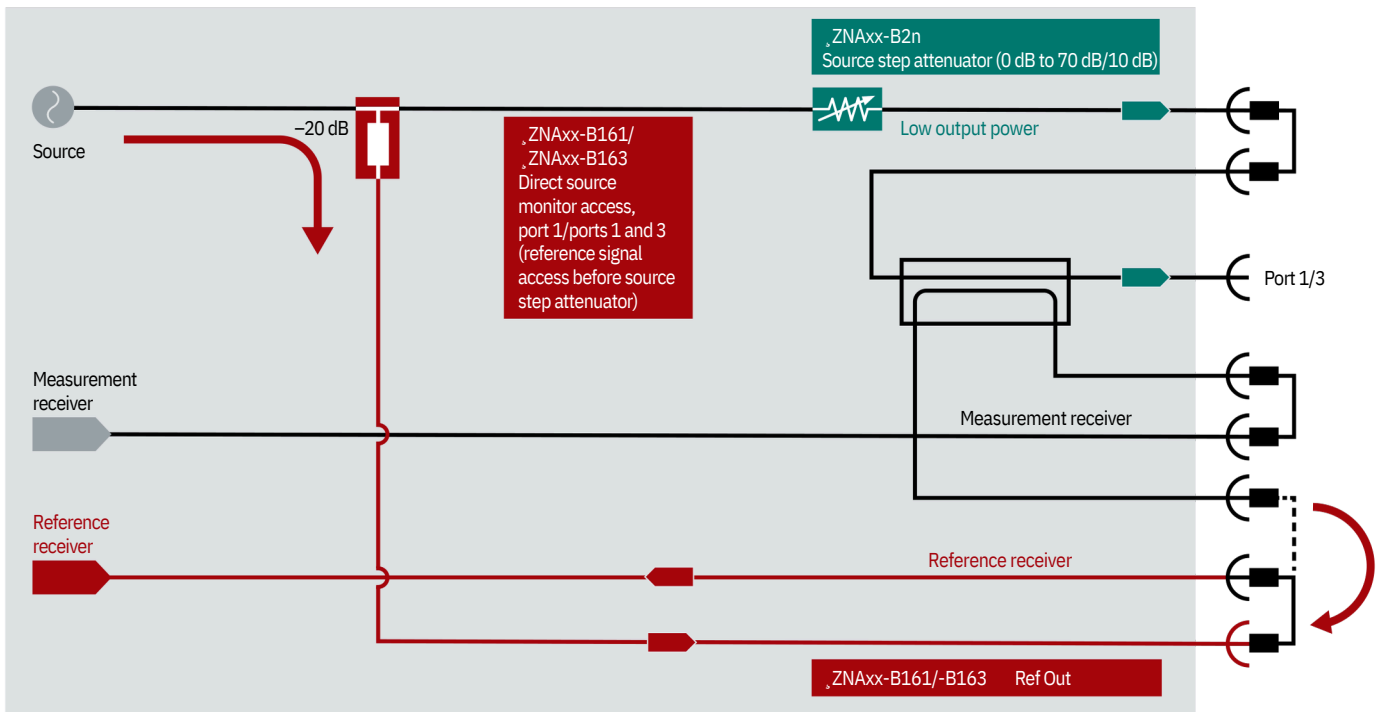
R&S®ZNAxx-B16 front panel jumper position required for direct source monitor access (R&S®ZNAxx-B161/-B163)

Internal preamplifier supports noise figure measurements

The R&S®ZNAxx-B302/-B312 option is a switchable low-noise amplifier (LNA) with filtering inserted upstream of the port 2 measurement receiver. With selectable gain up to 30 dB, even low gain/low noise figure DUTs can be accurately characterized.

R&S®ZNAxx-B161 and R&S®ZNAxx-B163 options

When the R&S®ZNAxx-B16 reference signal front panel jumper (ports 1 and 3) is reconnected from the standard position (Ref Out) to the direct source monitor output (R&S®ZNAxx-B161/R&S®ZNAxx-B163), the reference signal will be picked up before the source step attenuator.



UNPRECEDENTED RF QUALITY

Wide signal-to-noise ratio and exceptional stability for accurate results

Wide dynamic and power sweep range

The very high dynamic range of the R&S® ZNA allows the characterization of high-rejection filters. With high output powers and a wide power sweep range, the instrument can analyze the large- and small-signal behavior of amplifiers in a single sweep:

- ▶ Dynamic range: 147 dB (typ.)¹⁾, > 129 dB (specified, without options)
- ▶ Maximum attainable dynamic range: 170 dB (typ.)²⁾
- ▶ Electronically controlled power sweep range up to 100 dB (typ.), interruption-free up to 40 dB (typ.)

¹⁾ With R&S® ZNAxx-B3n option.

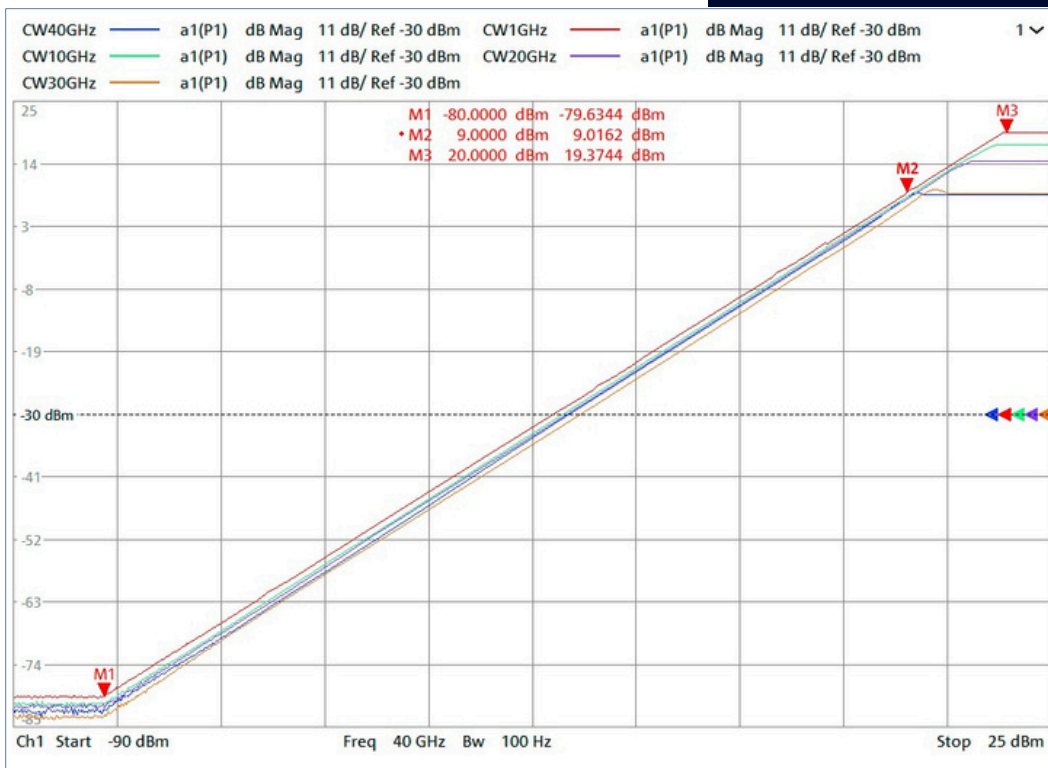
²⁾ Requires: maximum output power, R&S® ZNAxx-B16 option, R&S® ZNAxx-B3n option, reversed coupler configuration at receive port, and 1 Hz IF bandwidth.

High stability for reliable results

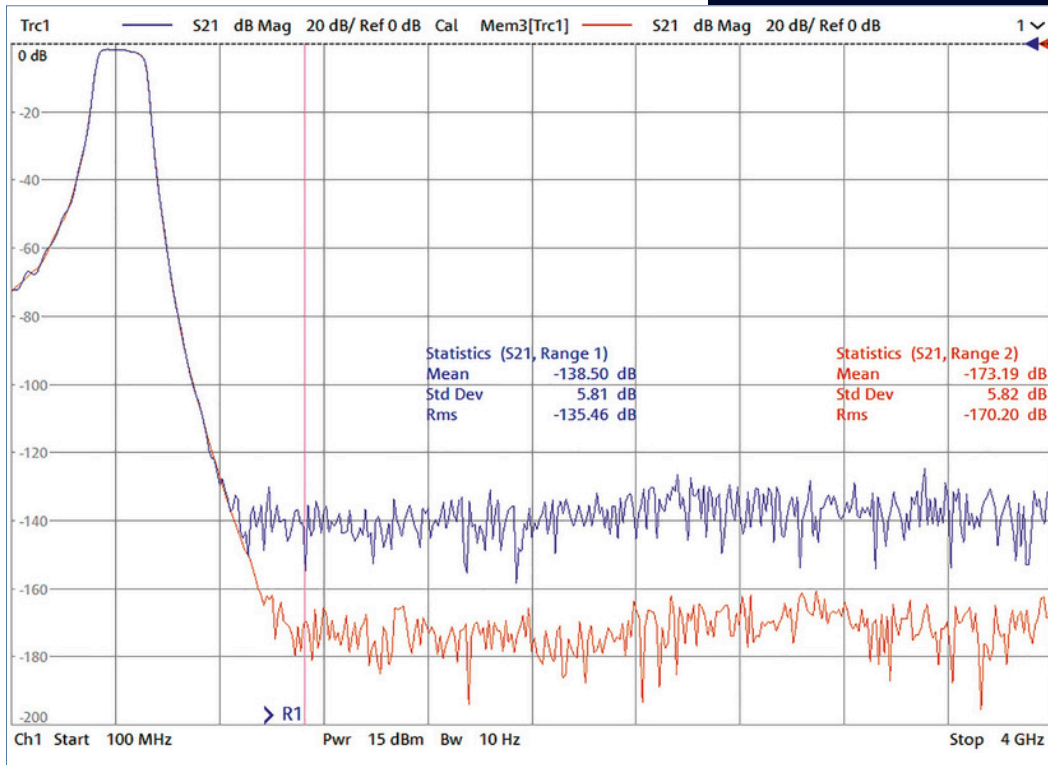
The R&S® ZNA testset and receivers feature excellent temperature and long-term performance stability. Combined with other decisive RF features, this offers outstanding reliability and accuracy.

- ▶ Trace noise of 0.001 dB (RMS, at 1 kHz IF bandwidth)
- ▶ Temperature stability of 0.01 dB/K and 0.1°/K
- ▶ Reliable measurement of high power levels thanks to 0.1 dB (typ.) receiver compression for 10 dBm power level at test port
- ▶ High dynamic range of sources due to source step attenuators up to 70 dB and electronic power sweep range up to 100 dB
- ▶ Excellent receiver linearity of < 0.03 dB (typ.) across an extremely wide range of -50 dBm to 0 dBm





Maximum power sweep range of up to 100 dB



Dynamic range: at maximum specified output power,
 without options (blue trace: at 10 Hz IF bandwidth);
 at maximum specified output power, in reversed coupler mode,
 with receiver step attenuator set to 0 dB (red trace: at 1 Hz IF bandwidth)

HARDWARE OPTIONS

| Description | Applications and benefits | Hardware option ¹⁾ |
|--|--|---|
| <p>Direct source and receiver access</p> <ul style="list-style-type: none"> ▶ With start frequency down to 100 kHz ²⁾ ▶ Supports reversed coupler configuration | <ul style="list-style-type: none"> ▶ Facilitates external test setups for high-power measurements across a wide frequency range ▶ Reversed coupler configuration increases dynamic range and reduces system noise figure | R&S®ZNAxx-B16 |
| R&S®ZNA 4-port model with up to four internal sources | <ul style="list-style-type: none"> ▶ No external sources means flexible configuration and short measurement times ▶ Flexible-to-configure, compact test setups, e.g. for DUTs with two converter stages | R&S®ZNAxx-B3 ³⁾ |
| <p>2nd internal LO source for 4-port R&S®ZNA model</p> <ul style="list-style-type: none"> ▶ For simultaneous measurement of two different frequencies (e.g. RF and IF signal of mixers) ▶ Additional RF source (in combination with R&S®ZNA-B8 mmWave converter LO output) | <ul style="list-style-type: none"> ▶ Fast mixer and converter measurements ▶ Very low trace noise with frequency-converting measurements ▶ General-purpose RF source up to 26.5 GHz (e.g. to provide LO signal for external mixers) | R&S®ZNA-B5 |
| 2nd internal RF source and 2nd internal LO source for 2-port R&S®ZNA model | <p>R&S®ZNA with 2 test ports supports:</p> <ul style="list-style-type: none"> ▶ Intermodulation measurements ▶ Group delay on embedded LO (satellite) converters (LNB), T/R modules ▶ Mixer tests (with R&S®ZNA-B8 for LO) | R&S®ZNA-B52 ³⁾ |
| Four/eight true receivers (no multiplexing) | <ul style="list-style-type: none"> ▶ Reliable multichannel phase and antenna measurements | Provided as standard in base unit (direct receiver access requires R&S®ZNAxx-B16) |
| Direct IF access, I/O ports switchable as inputs or outputs, with 2 GHz analog IF bandwidth (output) and 1 GHz analog IF bandwidth (input) | <p>Enhanced flexibility and sensitivity, e.g. when used in antenna test systems ▶</p> <ul style="list-style-type: none"> ▶ Provides direct access to up to eight phase coherent receivers ▶ Supports compact mmWave converter setups | R&S®ZNA-B26 |
| Eight internal pulse generators and four internal pulse modulators | <ul style="list-style-type: none"> ▶ For measurements on pulsed signals and for flexible system integration ▶ R&S®ZNA-B7 increases the number of wave quantities that can be captured in parallel with R&S®ZNA-K7 | R&S®ZNA-K7, R&S®ZNAxx-B4n ⁴⁾ , R&S®ZNA-B7 |
| Enhanced trigger and control functions (three additional trigger inputs, four trigger outputs, four pulse control I/O ports, ready for trigger, busy, RF interlock control) ⁵⁾ | <ul style="list-style-type: none"> ▶ Universal system adaptation and easy system integration ▶ High reference frequency for low phase noise | R&S®ZNA-B91 |
| Metrology configuration for R&S®ZNA | <ul style="list-style-type: none"> ▶ Enhanced long-term stability ▶ Support of 2/4-port R&S®ZNA | R&S®ZNAxx-B10 |
| Source step attenuators, 0 dB to 70 dB in 10 dB steps | <ul style="list-style-type: none"> ▶ Generation of low-power stimulus signals down to -110 dBm | R&S®ZNAxx-B2n ⁴⁾ |

¹⁾ xx designates the R&S®ZNA model (R&S®ZNA26, R&S®ZNA43, R&S®ZNA50 and R&S®ZNA67).

²⁾ Between 100 kHz and 10 MHz, the internal coupler can only be used to a limited extent. Here, external directional components and recalibration are required.

³⁾ The 2-port R&S®ZNA models come with one RF source as standard, the 4-port R&S®ZNA models with two RF sources.

⁴⁾ n designates the port number (1/2/3/4).

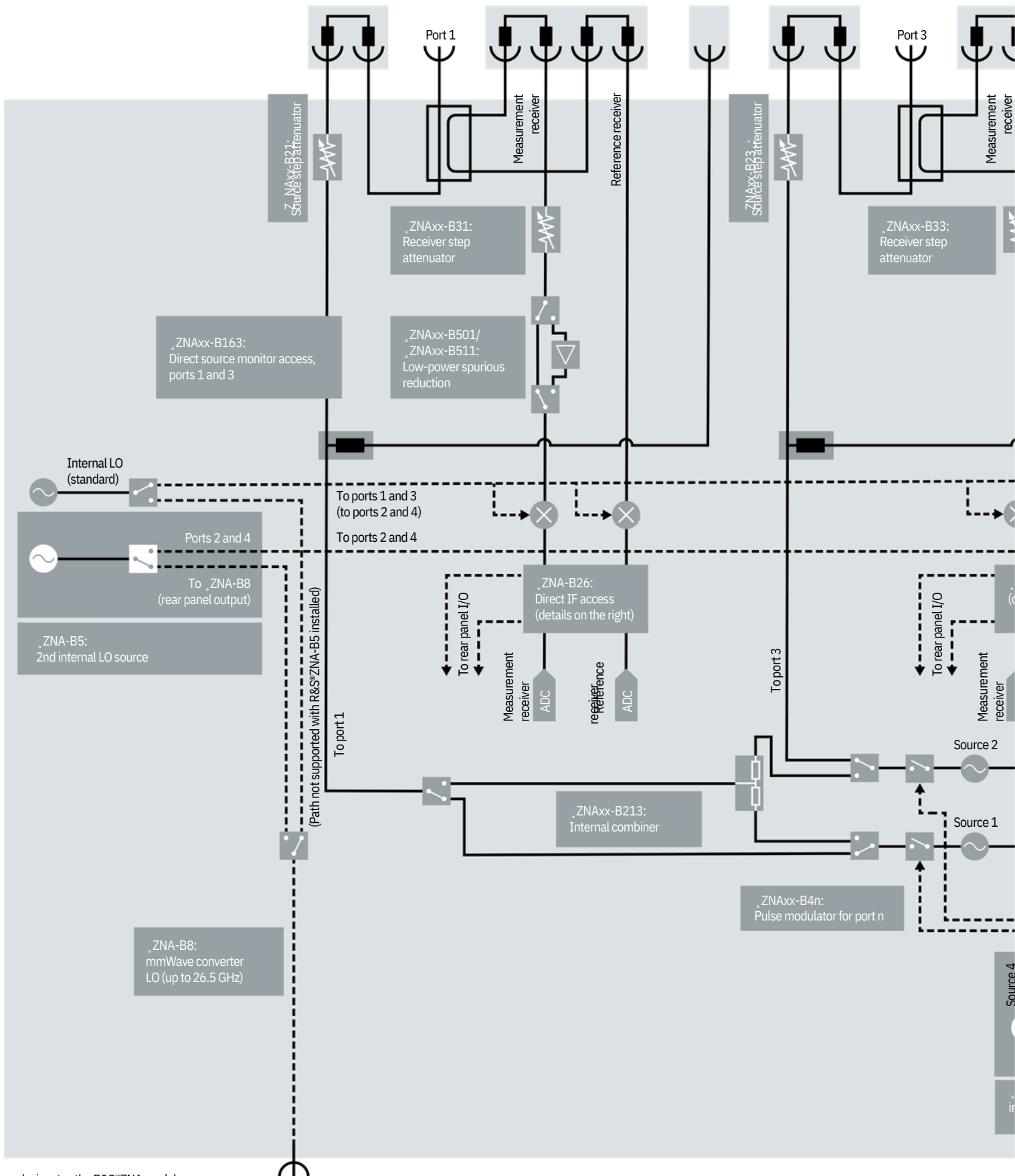
⁵⁾ 1 GHz reference frequency input provided as standard.

| Description | Applications and benefits | Hardware option ¹⁾ |
|--|--|--|
| Receiver step attenuators, 0 dB to 35 dB in 5 dB steps | <ul style="list-style-type: none"> ▶ Compression-free measurements with input power up to destruction limit of +27 dBm | R&S®ZNAxx-B3n ⁴⁾ |
| Rear panel output for internal LO signal (when the 2nd internal LO source (R&S®ZNA-B5) is installed, it is available at the output); provides up to +25 dBm output power | <ul style="list-style-type: none"> ▶ Support of compact mmWave converter setups (2/4 - port mmWave converter setups with 2/4 - port R&S®ZNA) without additional external source ▶ General-purpose RF source up to 26.5 GHz ▶ High source power not affected by hardware options installed in the R&S®ZNA frontend | R&S®ZNA-B8 |
| mmWave extender with LO output for R&S®ZNA67EXT ⁶⁾ | <ul style="list-style-type: none"> ▶ Enables frequency overrange above 110 GHz | R&S®ZNA-B80 |
| Frequency extension for R&S®ZNA67 | <ul style="list-style-type: none"> ▶ Frequency range extended up to 72 GHz ▶ Support of 2/4-port R&S®ZNA67 | R&S®ZNA67-B72 |
| Switchable internal combiner, provides a two-tone signal at port 1 | <ul style="list-style-type: none"> ▶ Intermodulation measurements ▶ Embedded LO converter group delay measurements (R&S®ZNA-K9 option) ▶ Mixer measurements with 2-port R&S®ZNA models (R&S®ZNA-B8 as 26.5 GHz LO source) | R&S®ZNAxx-B213 for 4-port models, R&S®ZNAxx-B212 for 2-port models |
| Direct source monitor (reference signal) access; when reconnecting the R&S®ZNAxx-B16 reference signal front panel jumper to the direct source monitor output (R&S®ZNAxx-B161/-B163), the signal to the reference receiver can be picked up before the source step attenuator | <ul style="list-style-type: none"> ▶ Low trace noise even with low output power levels as typically encountered with high gain DUTs ▶ Monitoring of source output power simultaneously at source monitor output and test port | R&S®ZNAxx-B161, R&S®ZNAxx-B163 |
| Low-noise preamplifier at port 2 measurement receiver, switchable low-noise amplifier (LNA) with selectable gain and integrated filter | <ul style="list-style-type: none"> ▶ Noise figure measurements on amplifiers and converters ▶ Up to 30 dB gain for low gain / low noise figure DUTs | R&S®ZNAxx-B302 ⁷⁾ , R&S®ZNAxx-B312 |
| Low-power spurious reduction, isolation amplifier at port 1 measurement receiver; low-power spurious level is reduced down to -110 dBm | <ul style="list-style-type: none"> ▶ Optimized spurious suppression ▶ Signal purity with very low stimulus levels ▶ Reliable high gain amplifier/converter testing | R&S®ZNAxx-B501 ⁶⁾ , R&S®ZNAxx-B511 |
| Direct control interface, a proprietary interface for Rohde & Schwarz extensions | <ul style="list-style-type: none"> ▶ Control of R&S®ZN-ZCG comb generator as phase reference ▶ Control of the external RFFE GPIO interface ▶ Control of switch matrices such as R&S®ZN-Z8x | R&S®ZNA-B12 |
| MIPI RF frontend (RFFE) and general-purpose input/output (GPIO) interface, including voltage and current measurements | <ul style="list-style-type: none"> ▶ Integrated, configurable control of mobile phone frontend chipsets ▶ Additional digital and analog I/O | R&S®ZNA-B15 |

⁶⁾ Export restricted.

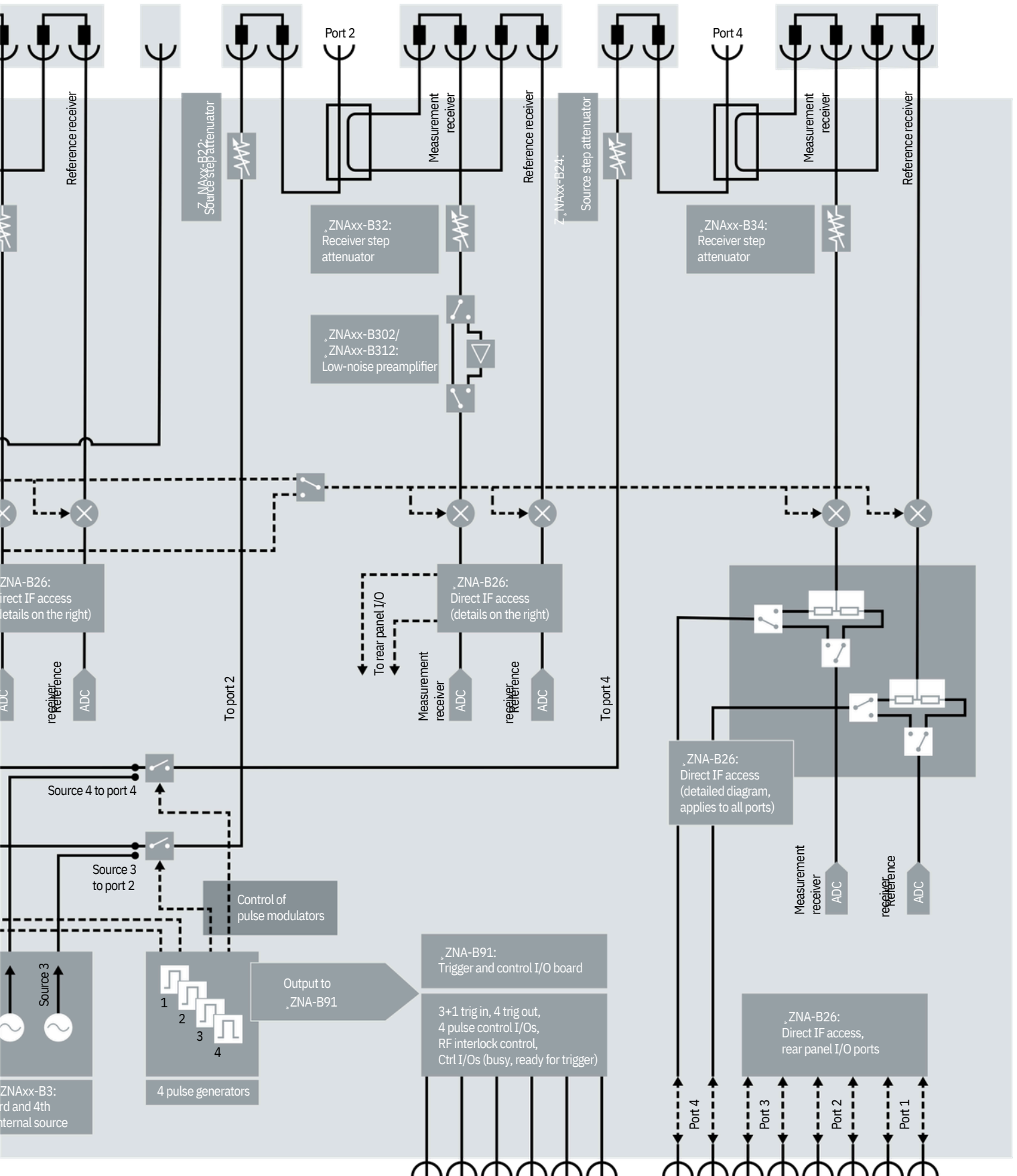
⁷⁾ R&S®ZNAxx-B302 and R&S®ZNAxx-B501 options provoke increased receiver sensitivity for other option(s). If the enhanced sensitivity conflicts with country-specific export regulations, R&S®ZNAxx-B312 and R&S®ZNAxx-B511 options can be ordered instead.

PRINCIPLE OF OPERATION OF 4-PORT R&S

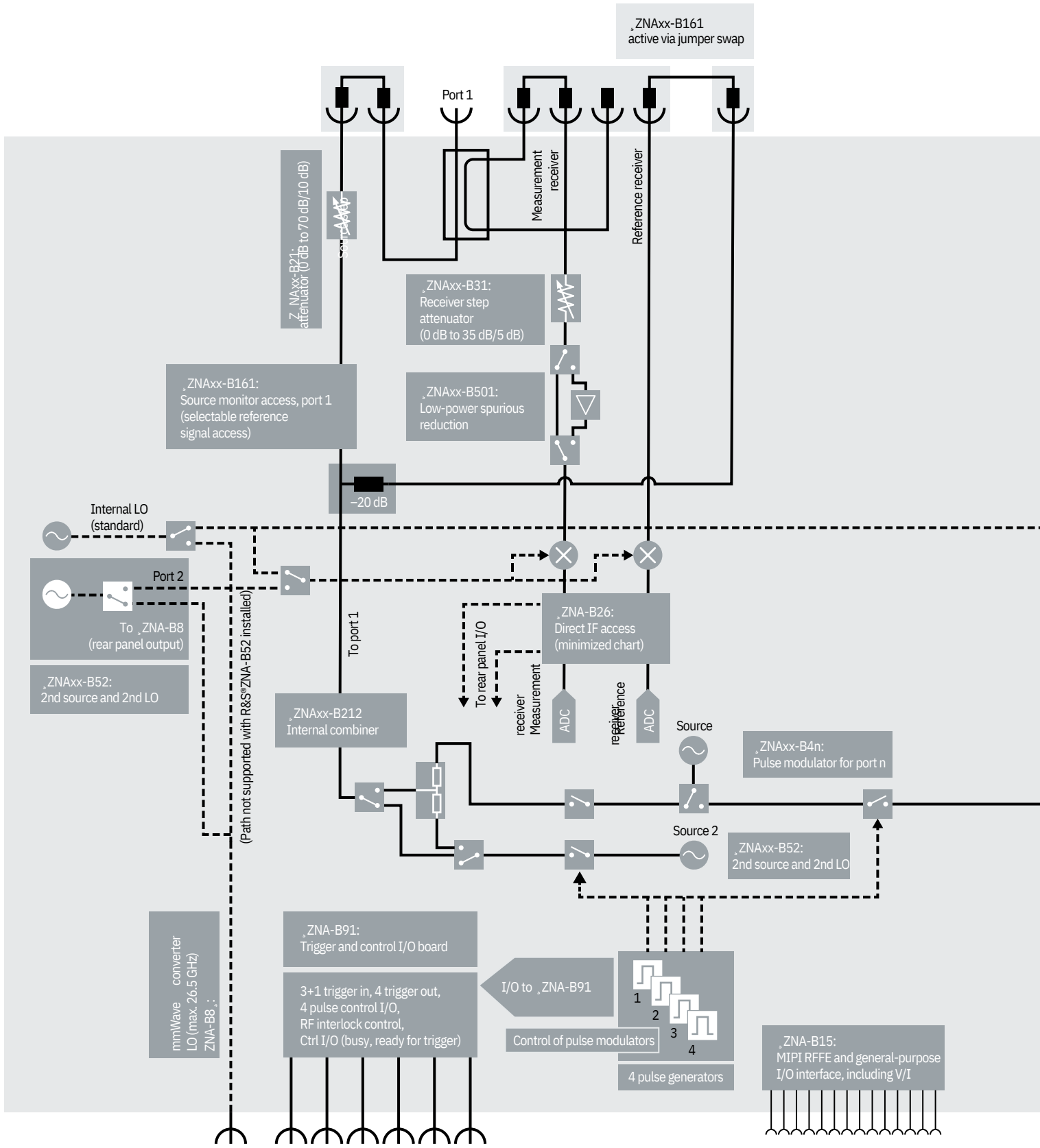


xx designates the R&S®ZNA model.
n designates the port number (1/2/3/4).

„ZNAxx-B16 option: Direct source and receiver access
(frequency extension down to 100 kHz, supports reversed coupler operation)

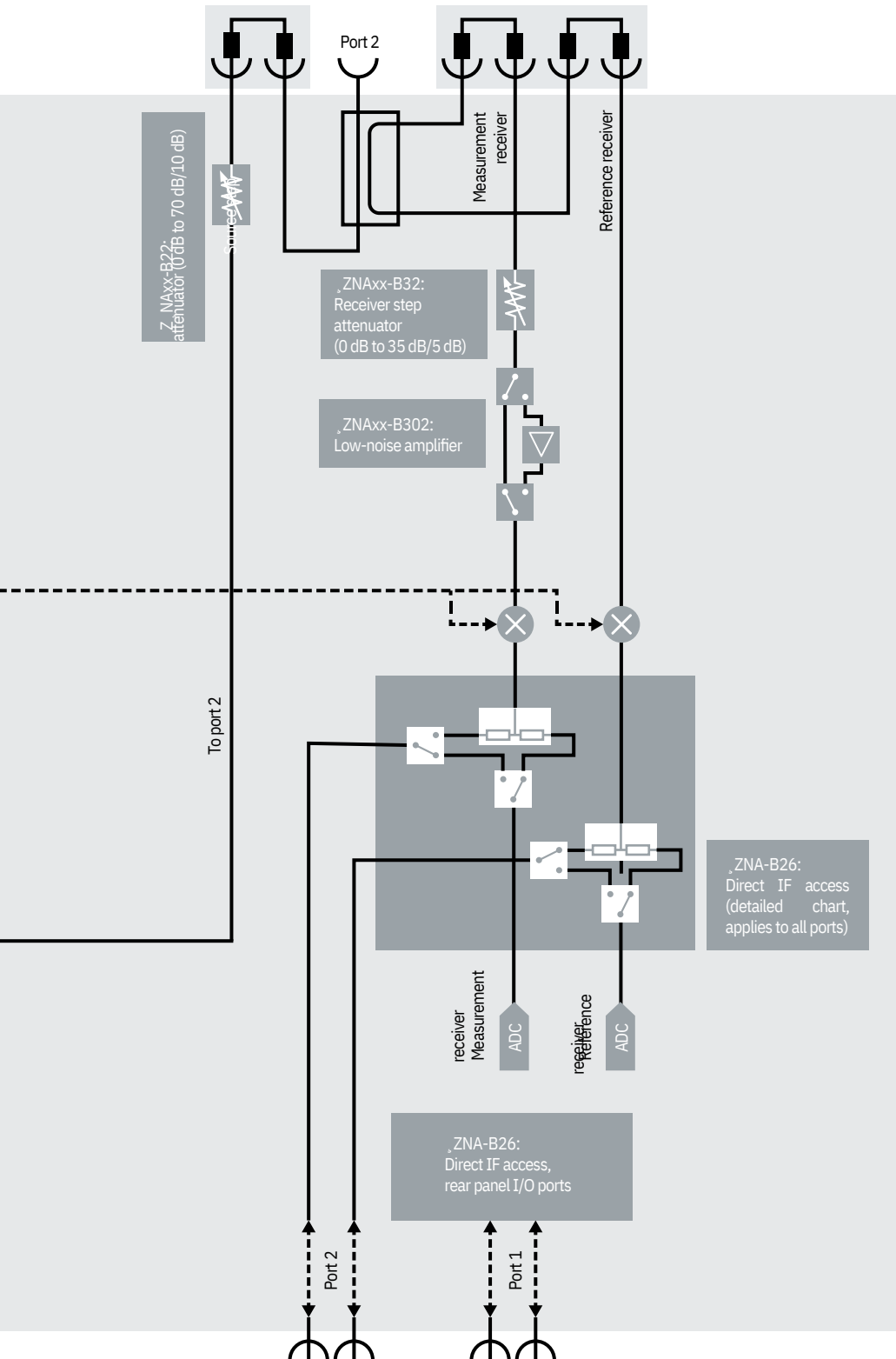


PRINCIPLE OF OPERATION OF 2-PORT R&S



xx designates the R&S®ZNA model.
n designates the port number (1/2).

ZNAxx-B16option:
Direct source and receiver access (includes 100 kHz start frequency)



THE RIGHT CALIBRATION FOR EVERY TEST SCENARIO

The R&S®ZNA offers a wider range of calibration techniques for coaxial and non-coaxial systems, such as wave guides and printed circuit boards (PCB). Various deembedding techniques offer solutions for in-fixture and on-wafer calibration. The R&S®SMARTerCal concept combines system error correction with receiver and flatness calibration, guiding the operator efficiently to the optimal result.

Full calibration with only three standards – faster, simpler, more precise

- ▶ Through, reflect, line/line, reflect, line (TRL/LRL) for on-wafer applications, waveguides and coaxial DUTs
- ▶ Through, reflect, match (TRM) for applications in test fixtures and on wafers
- ▶ Through, short, match (TSM) and through, open, match (TOM) as alternatives to TOSM, for reduced calibration effort

Calibration for DUTs using a mix of connectors

The classic TOSM method does not provide direct calibration of test setups for DUTs equipped with different types of connectors at the input and output. The R&S®ZNA offers two alternatives to provide this type of calibration.

UOSM calibration

Unknown through, open, short, match (UOSM) calibration is the smartest way to overcome the above problem. It involves about the same effort as TOSM calibration. A through connection with unknown parameters is required, i.e. a reciprocal (but otherwise more or less arbitrary) two-port, e.g. a simple and cost-effective adapter.

Adapter removal method

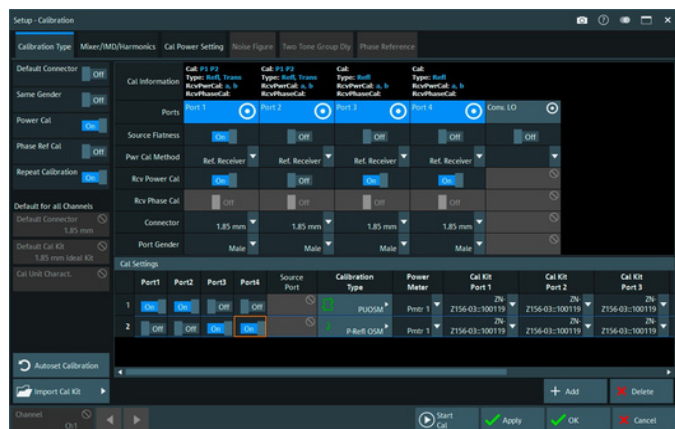
The R&S®ZNA also provides classic adapter removal calibration. This method is very robust, but requires many more calibration steps.

R&S®SMARTerCal – get ready for active device testing

Calibrating the absolute power levels of the sources and receivers is indispensable in order to reliably test amplifiers, mixers and T/R modules. However, this process is time-consuming. The R&S®ZNA uses a special calibration technique referred to as R&S®SMARTerCal, which radically simplifies calibration. R&S®SMARTerCal combines the information gained from system error correction (e.g. TOSM, UOSM) with the information obtained through absolute power level calibration (wave quantities in terms of amplitude and phase). This means that the absolute power levels of the sources and receivers are calibrated already during system error correction, taking into account port mismatch. For absolute output power level calibration, the power sensor needs to be connected to a test port only once. The calibration values for all other sources and receivers are derived from the calibration values for that specific test port. This significantly reduces calibration time and effort.

Multiline TRL calibration in line with National Institute of Standards and Technology (NIST)

Even though standard TRL calibration is preferable for on-wafer calibration or planar line systems, NIST multiline TRL calibration has valuable features that improve accuracy and reliability. The calibration is in line with NIST recommendations and can overcome standard TRL frequency band limitations while avoiding the potential discontinuities in the transition frequencies when several TRL bands are concatenated. Taking line attenuation into account further increases accuracy. The use of multiple lines also creates optimized calibration over a wide frequency range.



The R&S®SMARTerCal merges system error correction, receiver power calibration and absolute source level calibration.

Digital automatic level control (ALC)

The configurable digital ALC sets the source power precisely to the target value, using a reference signal that can be derived from any point in the test setup. This means that the source power is adjusted, in a minimum of time, to the output power of a preamplifier in the test setup or to the output power of the DUT. Power fluctuations, e.g. due to drift effects, are eliminated. This provides stable, reproducible power conditions over long test cycles.

Unlike wideband diode detectors, the ALC uses the digitally filtered results delivered by the reference receivers. As a result, the source power is adjusted to the power of the wanted signal (fundamental) without any distortion otherwise introduced by harmonics, for example. Users can configure the ALC parameters, such as the ALC IF bandwidth, to achieve the optimum balance of accuracy and control time.

ALC controlled high-power setups

With the reference signal picked up at any point in the test setup, the R&S®ZNA controls the source to keep output power from booster amplifiers stable with high precision. Settling effects are equalized in milliseconds and measurements can be triggered immediately after power changes.

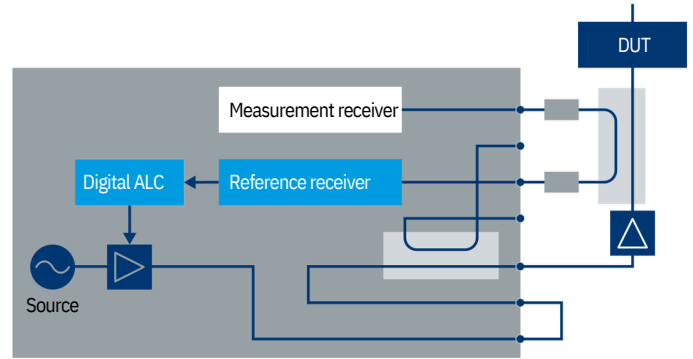
ALC ensures accuracy at very low levels

The analyzer's excellent receiver linearity of < 0.05 dB across a wide range from -50 dBm to 0 dBm results in high level accuracy even when measuring very low power levels. The receivers are calibrated at a higher power level that is optimal for the power sensor. The power level is then reduced, while power accuracy is maintained thanks to the reference receivers' high linearity and ALC control.

Amplifier IM and converter test

For measurements requiring two or more signals, (intermodulation test, R&S®ZNA-K9 converter group delay test) all sources involved are controlled for reliable active device characterization.

Digital automatic level control (ALC)



ALC operation: in a high-power setup with an external preamplifier and a directional coupler, the source power is controlled to match the preamplifier output power. This compensates for drift effects, making the output power very precise and stable.

ALC deembedding for in-fixture and on-wafer noise figure tests

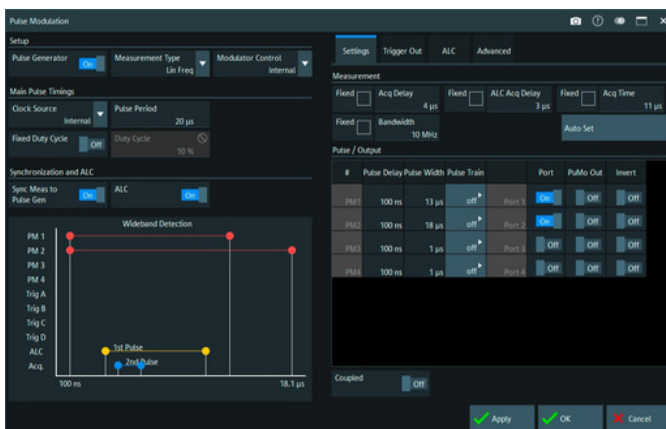
The ALC accounts for deembedded virtual networks, inserted or removed after power calibration. This way, the reference plane for the power control is shifted at the end of probes for the on-wafer test or into test fixtures. The latter is particularly useful for noise figure measurement for in-fixture/on-wafer chip tests.

ALC with pulsed signals

The finite measurement and control time of the ALC is typically longer than the short pulse duration time. To find the optimal setting, the ALC and pulse parameters can be matched, and users can select whether to carry out ALC control and measurement on the same or on successive pulses.

Power offset correction for short pulses

The point-wise ALC cycle may result in a total control and measurement time per point that exceeds the duration of the short pulses. As an alternative, R&S®ZNA offers a sweep-wise power offset correction, where the power is corrected after the completion of each sweep. Thus, the measurement IFBW is decisive for the time per point, without time offset.



The configuration of ALC supported measurements under pulsed condition allows detailed settings to match ALC and pulse parameters. For instance, to allow short pulses, ALC control and measurement can be set to successive pulses.

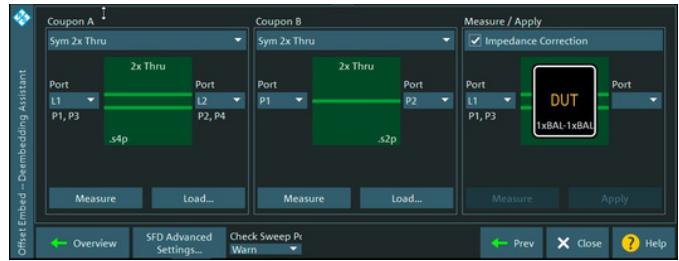
Fast deembedding for impedance matching using virtual networks

Coaxial and balanced components, such as surface acoustic wave (SAW) filters used in mobile phone frontends, are specified together with the networks that match them to the impedance of the surrounding circuit. The R&S®ZNA can embed the DUT into virtual matching networks to provide realistic conditions by simulating the DUT installed in its operational environment. The R&S®ZNA offers a choice of predefined matching network topologies. If values of individual network elements are edited, the R&S®ZNA immediately recalculates the network and embeds the DUT in the new network in real time. In addition to predefined topologies, .s2p, .s4p, .s6p and .s8p files can be read into the R&S®ZNA and used for embedding/deembedding.

Enhanced solutions for in-fixture and PCB testing

If DUTs do not have coaxial connectors, vector network analyzer calibration often cannot be made directly in the reference planes. This is the case for in-fixture and on-wafer chip tests, measurements of PCB structures, non-coaxial connectors or cables and all non-connectorized components. In these cases, test fixtures, probes or other structures are used to adapt from the coaxial interface at the calibration plane to the device under test. The corresponding lead-ins and lead-outs need to be modelled and characterized via their S-parameters, so that they can be deembedded from the measurement results.

For such tasks, the R&S®ZNA is prepared by seamless integration of third-party tools made available as the R&S®ZNA-K210, R&S®ZNA-K220, R&S®ZNA-K230 and R&S®ZNA-K231 options. All procedures are coupon based, and differ by the type and number of applied test coupons, the incorporation of PCB impedance effects, and calculation speed. A user-friendly wizard with a graphical interface and parameter entries specific to each deembedding tool, guide the operator through the entire calibration and deembedding procedure.



For in-fixture and PCB tests Rohde & Schwarz offers advanced coupon based deembedding options, supported by a smart configuration wizard.

Calibration equipment

The R&S®ZN-Z1xx economy calibration kits provide robust operation up to 43.5 GHz. The R&S®ZN-Z2xx high-end calibration kits are available for more sophisticated requirements, offering calibration standards from type N through 1.0 mm (110 GHz connectors). These kits achieve very high calibration accuracy thanks to precision manufacturing combined with S-parameter based characterization of the individual calibration standards.

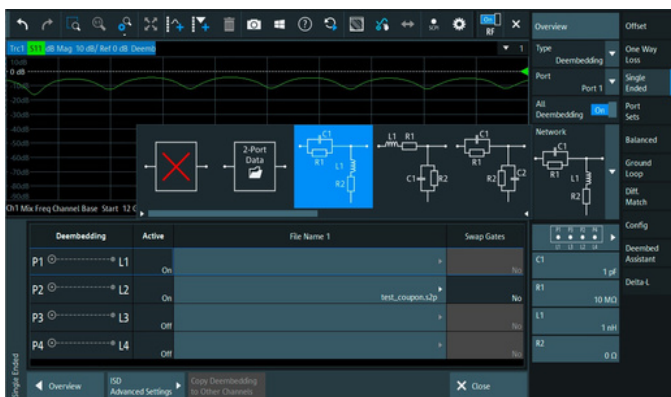
Automatic calibration units

Automatic calibration units up to 67 GHz with two or four ports greatly simplify calibration, while reducing operator errors and improving calibration repeatability.

Calibration of mixer and converter setups

With the R&S®ZNA-K4, R&S®ZNA-K5 and R&S®ZNA-K9 options, the R&S®ZNA supports comprehensive characterization of frequency translating devices, such as mixers, T/R modules, and (embedded LO) satellite receivers (LNB). For the R&S®ZNA to measure group delay and, for instance, transmission phase, the mixer used for calibration should be reciprocal in corresponding limits. Users can extend their manual kit or calibration unit with calibration mixers that meet this requirement. The R&S®ZN-ZM292 is reciprocal¹⁾ within tight limits and covers common conversion schematics up to 40 GHz.

¹⁾ Ideal reciprocity and thus the absolute phase accuracy is degraded by S21/S12 uncertainty, and LO contributions.



The R&S®ZNA comes with a choice of predefined matching networks whose values can be edited. If values are changed, the R&S®ZNA will immediately recalculate the network and embed the DUT in the new network in real time.



R&S®ZN-ZCG44/67 comb generator, for calibration of phase reference



R&S®ZN-Z1xx economy calibration kit



R&S®ZN-Z2xx high-end calibration kits



R&S®ZN-Z156 calibration unit

R&S®ZN-ZCG comb generator

The R&S®ZN-ZCG comb generator has a traceable wide-band phase reference for calibrating R&S®ZNA receivers that enables phase-accurate harmonic and sideband measurements of power amplifiers and frequency-converting DUTs such as mixers and converters. The R&S®ZN-ZCG generates a pulse train with a dense set of equally spaced comb lines in its spectrum. The magnitude and phase of each line are characterized in the factory. R&S®ZNA receiver channels for a test-port group can be prepared for wideband phase testing.

The R&S®ZNA-B12 device control interface handles synchronization and control by using a 2 GHz clock from a R&S®ZNA test port during calibration.

Tone spacing can be selected in the kHz range up to 100 MHz with additional user-defined spacing available up to 2 GHz to closely match the measurement frequency grid and maximize the signal-to-noise ratio (SNR) for comb lines. The R&S®ZN-ZCG44 and R&S®ZN-ZCG67 cover frequencies up to 44 GHz respectively 67 GHz and NIST traceability ensure reliability.

The comb generator is supported by R&S®SMARTerCal and can be used as a calibration unit. The comb generator can also be disconnected after error correction, leaving all test ports available for measurements. The generator can also be monitored when operating or used as a stand-alone unit in nonlinear, large-signal setups.

Real-time measurement uncertainty and verification

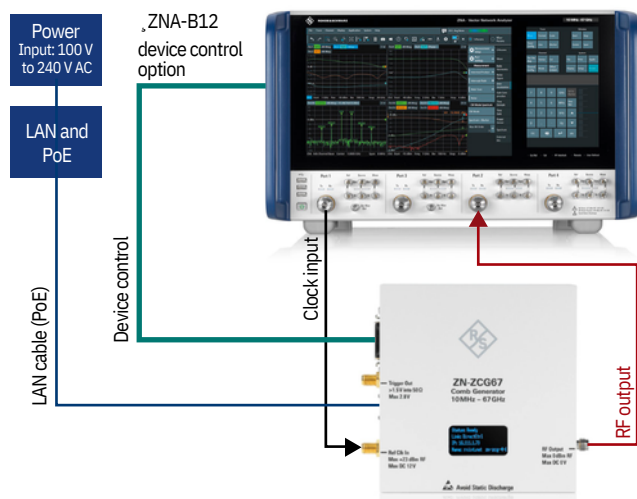
Uncertainty data listed on data sheets is inevitably provided for only a limited set of test parameters. With the two functionalities offered by the R&S®ZNA-K50(P) option, operators can check uncertainty under the given test conditions and verify actual RF performance:

- ▶ S-parameter traces can be displayed with error bars, calculated in real time depending on the current settings
- ▶ Verification measurements are performed to ensure that verification standards match their characterization values. Utilizing R&S®ZV-Z4xx verification kits ensures traceability of measurement results to the Swiss metrology authority METAS.

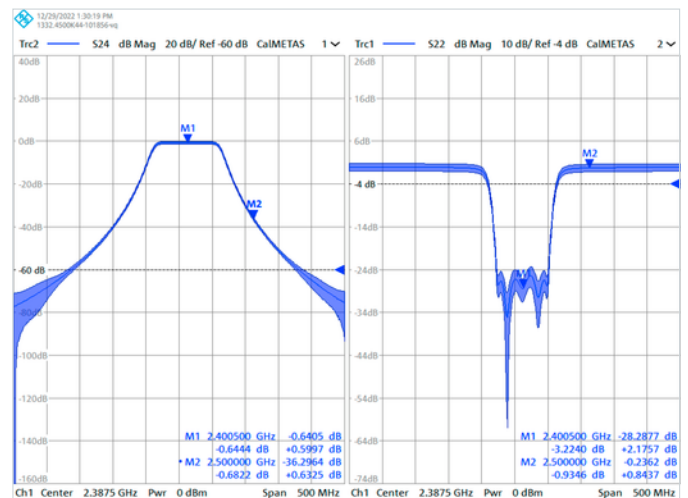
The R&S®ZNA-K50(P) option requires installation of the VNA tool from the Swiss metrology authority METAS. This option enables operators to use the VNA tool as an additional means of individual uncertainty evaluation.

R&S®ZN-ZCG connection example for R&S®ZNA calibration

The R&S®ZN-ZCG44/67 calibration setup has one RF port feeding the 2 GHz clock signal. When combined with the R&S®SMARTerCal, all receivers are phase-calibrated. The R&S®ZN-ZCG can be disconnected after calibration, as with a calibration unit.



R&S®ZNA-K50(P) option adds error bars to S-parameter traces in real time, to calculate the uncertainty in real time for every sweep.



HIGH-END, APPLICATION-TAILORED PERFORMANCE

Along with basic RF performance, smart features optimize test setups and test execution.

Features for quick results

Besides very short measurement times, the R&S®ZNA has other features to speed up data acquisition. The specified high dynamic range of > 129 dB generates a high SNR for accurate measurements, even with large IF bandwidths and it only needs short amount of time for measurements. RF and IF signals can be recorded simultaneously with the second internal LO source when measuring mixers. Measurement speeds are fast enough to measure non-frequency-converting S-parameters. The R&S®ZNA can pick up measurement data on all of its ports simultaneously for parallel testing of two 2-port DUTs, doubling throughput.

Flexible multiportsystems with speed enhancement

Besides active device characterization, passive device and digital design testing (DDT) is challenging for multi-band and multiport testing due to high port numbers and sweeps with large point counts. The R&S®ZNA-K66 option for a 4-port R&S®ZNA significantly improves speed while letting users reduce sweep time and maintain measurement quality.

Combining the R&S®ZNA with one or more configurable R&S®OSP open switch and control unit supports multiport measurements. The R&S®ZNRun vector network analyzer test automation suite is a powerful software tool that makes defining a test configuration easy. The software suite was designed for optimization and acknowledges that workflows need to be expedited as much as possible.



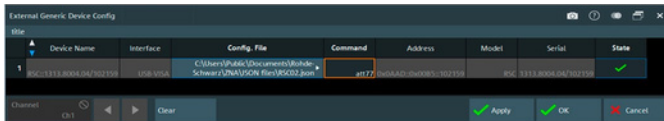
R&S®ZNA based multiport solution for fully automated multiport testing; highest flexibility is provided by integrating the configurable R&S®OSP320 open switch and control units.

SYSTEM INTEGRATION AND CONNECTIVITY

Flexible test system completion with user instrumentation, extended dynamic link library (DLL) and remote instrument monitoring.

Generic device system integration

The R&S®ZNA supports a wide range of auxiliary instruments by default, such as Rohde & Schwarz signal generators and power test heads. If the test system needs to be extended with further instrumentation, the R&S®ZNA firmware provides the operator a powerful and flexible tool by means of external generic device configuration. With command files in JavaScript Object Notation (JSON, *.json) format, users can set up communications to an external VISA capable device. ASCII notation can be used to define sequences of commands, and command files for different instruments can be loaded.



A JSON command list file is defined in the "External Generic Device Config" menu. A command or command sequence from the file can be selected for each channel.

Dynamic link library integration

An even more powerful and versatile tool is the integration of user-provided DLL. Besides the control of external devices, (firmware compatible) GUI windows can be created, and individual data processing and analysis can be added. A basic example is the control of an external power meter or source monitor unit for an amplifier power added efficiency measurement (PAE). For some Rohde & Schwarz power meters, plug & play DLLs are available, and the open DLL architecture supports operators who want to integrate custom code.

Health and utilization monitoring service (HUMS)

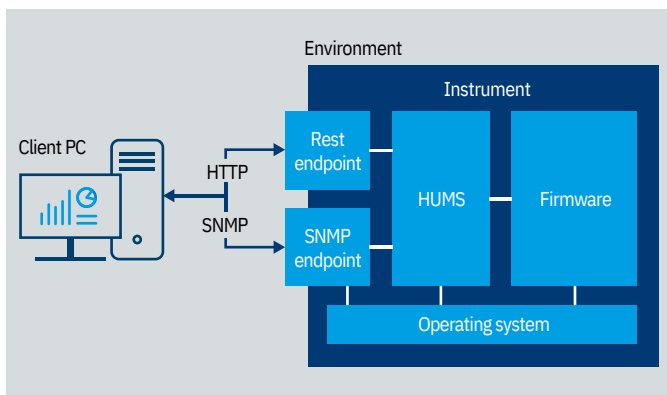
For companies with a large installed instrument base and extended networks, a clear overview of the entire network and central management is crucial for ensuring effective and reliable operations across the network. The software for all of the modules needs to be kept up to date, costs and efficiency need to be optimized using statistical data, operations need to be monitored and failures recognized as soon as possible. HUMS is a service that runs locally on each instrument, collecting and storing data on that instrument. Data can be retrieved by standard plug & play browser based communications, and with application specific programming.

HUMS is available on the R&S®ZNA with the R&S®ZNA-K980 software option. HUMS opens the SNMP agent and a REST service with HTTP endpoints, which allows the HUMS data to be retrieved.

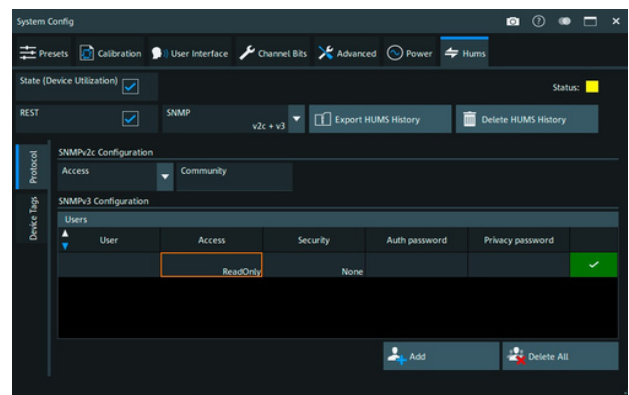
Some examples of parameters obtainable from a VNA:

- ▶ Hardware and software options
- ▶ Detailed info on hardware components (e.g. sync, HDD)
- ▶ Status (self-test, system messages, service)
- ▶ Malware status
- ▶ Storage capacity
- ▶ Utilization (e.g. activity of hardware and software options, count number of switching cycles)

Functional schematic of HUMS



R&S®ZNA HUMS activation and configuration GUI



MEASUREMENT MODES



COMPRESSION POINT MEASUREMENTS

Determining the compression point is essential when characterizing active components. With the R&S®ZNA, compression point measurements can be flexibly combined with S-parameter measurements.

Highly accurate results

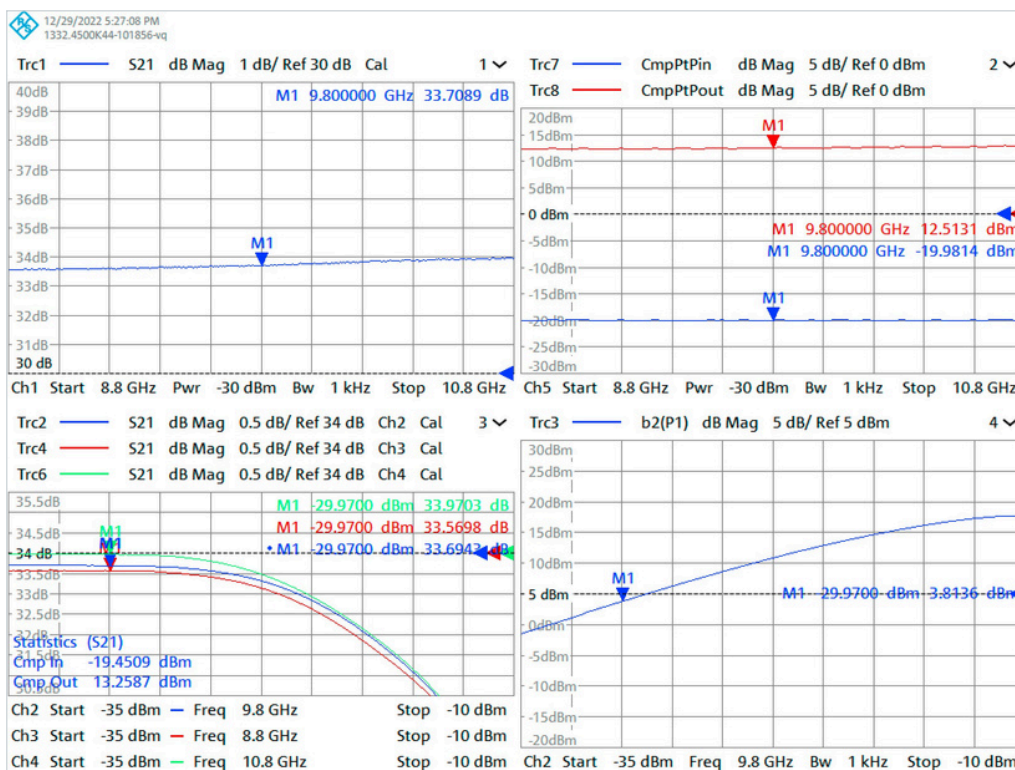
Compression measurements in particular require accurate power levels for stimulation and measurement as well as port match correction. The R&S®SMARTerCal procedure combines receiver power calibration, source flatness calibration and system error correction, thus compensating for the test set response and system error. Outstanding high receiver linearity makes it possible to reduce power calibration to a single point of the power sweep, which drastically reduces calibration time.

Power and phase sweeps for detailed insight

To find the optimum set of power sweep parameters, single power sweeps at dedicated frequencies can be combined in one display. For single power sweeps, the x dB (where x dB is typically assumed as 1 dB or 0.1 dB) compression can be flexibly referenced to single values or power ranges, thus minimizing noise effects in the small signal range. Compression power and S-parameters are shown in real time. The reverse power sweep reveals hysteresis effects of the DUT and the test time can be reduced by the swept mode.

Compression versus frequency

Automatic compression measurement performs power sweeps in the background at each data point and directly shows the CP(f) in terms of the input/output power or as an S-parameter. To minimize measurement time, the linear range can be skipped by defining a back-off value to set a reference different from the power sweep start value.



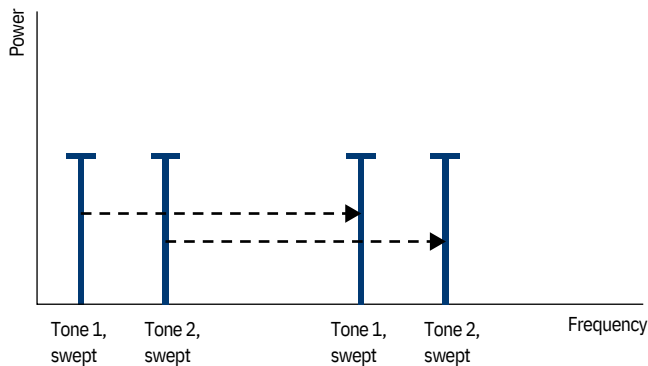
Amplifier compression measurements:

- ▶ Gain
- ▶ Compression point by measurement of power sweeps at dedicated frequencies
- ▶ Input and output power compression point versus frequency
- ▶ Absolute power

INTERMODULATION MEASUREMENTS ON AMPLIFIERS AND MIXERS

The R&S®ZNA makes it possible to determine the intermodulation characteristics of amplifiers and mixers fast and with high accuracy.

Frequency sweep with fixed carrier spacing



The R&S®ZNA provides the following three types of intermodulation measurements:

- ▶ Frequency sweep with fixed carrier spacing
- ▶ Frequency sweep with variable carrier spacing
- ▶ Power sweep with fixed carrier spacing

Wide dynamic range and digital ALC for challenging intermodulation measurements

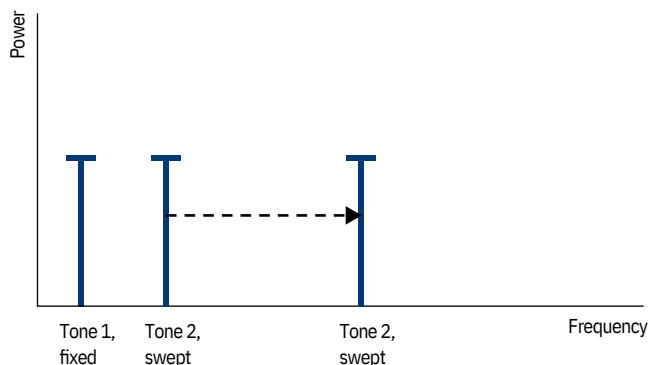
The R&S®ZNA offers major benefits especially when measuring amplifiers with very small intermodulation products. Its wide dynamic range and the excellent power handling capacity of its receivers make it possible to measure low intermodulation distortion within seconds instead of minutes.

When measuring intermodulation, precise control of the powers applied to the DUT inputs is vital. Here, the R&S®ZNA makes no compromises. Automatic level control (ALC) combined with system error correction ensures a precise amplitude for the individual carriers over the entire frequency range, regardless of the DUT's input reflection coefficient.

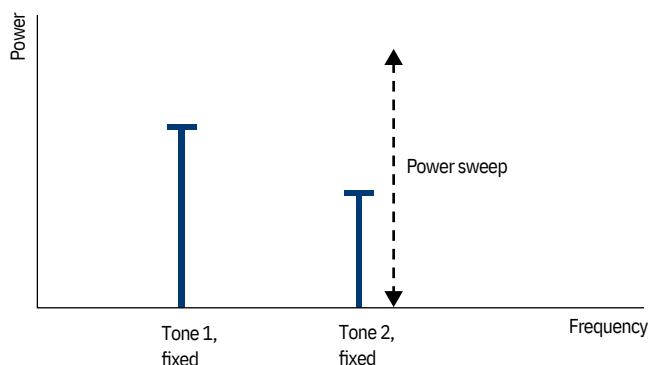
High output power and flexibility

Featuring four independent sources, the R&S®ZNA can even perform intermodulation measurements on mixers without requiring an external source. The analyzer delivers high output powers of up to +20 dBm per test port. If this is not sufficient, the R&S®ZNA can flexibly loop external amplifiers into the signal path and precisely control them via ALC.

Frequency sweep with variable carrier spacing

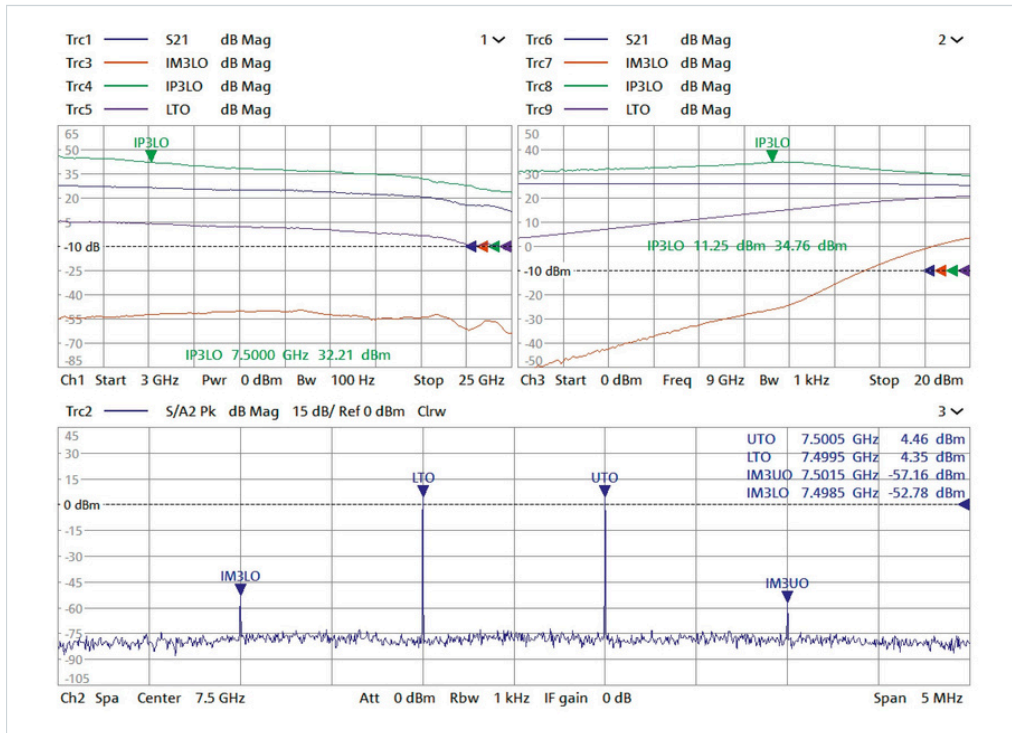


Power sweep with fixed carrier spacing

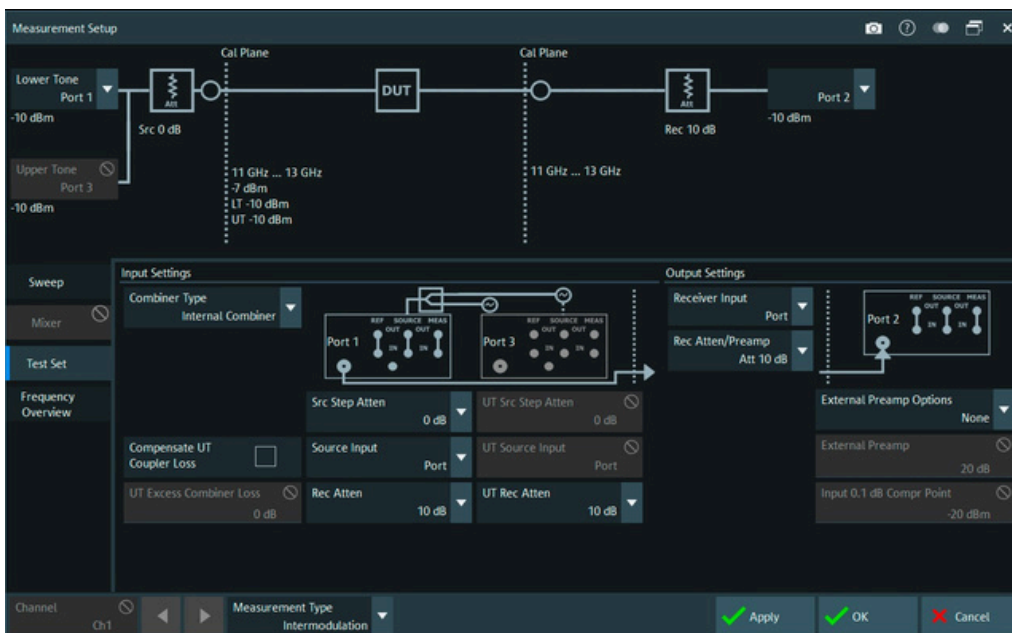


Simplified configuration with graphical user interfaces

Dedicated mixer and intermodulation tests can be configured with tailored GUIs. The test parameters are displayed at corresponding positions in a test set diagram. The actual hardware settings for attenuators and (direct) channel access ports are dynamically displayed above the diagrams, so that operators can keep track and be confident about the setup and test results.



Comprehensive amplifier characterization, including intermodulation products (IP), IP versus frequency, spectral measurements and other quantities



Configuration GUI for an amplifier intermodulation test

NOISE FIGURE MEASUREMENTS ON AMPLIFIERS AND MIXERS

The R&S®ZNA-K30 noise figure measurement option further enhances the R&S®ZNA to provide a powerful and versatile test system for full characterization of amplifiers and converters.

Noise figure measurement on amplifiers and mixers

The R&S®ZNA-K30 noise figure measurement option expands the R&S®ZNA to include noise figure analysis for amplifiers, converters and T/R modules. Hardware options can be added to further optimize this functionality, e.g. to stimulate high gain amplifiers with very low levels or to measure low gain/low noise figure LNAs with high accuracy.

Single connection device characterization

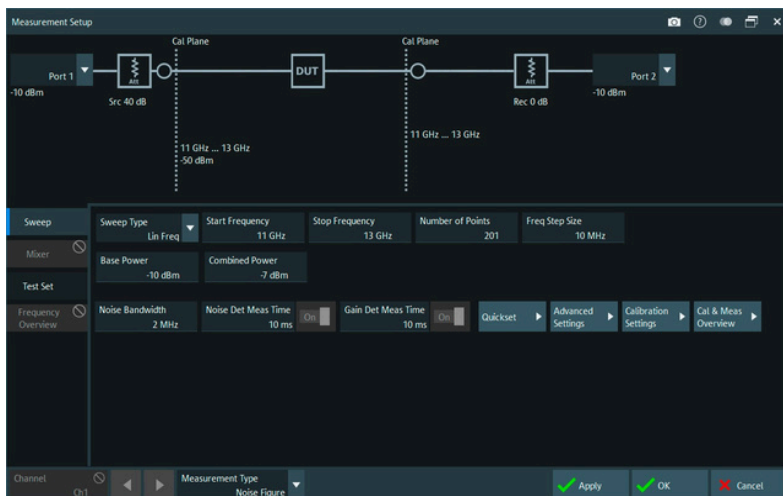
Instead of using a noise source to determine the noise figure, the R&S®ZNA directly measures absolute noise power, based on absolute power level calibration and system error correction. Likewise, instrument calibration with a manual calibration standard, a calibration unit and a power sensor requires no extra equipment; an external noise source is not necessary. The calibration process is included in the convenient calibrate all function for the entire setup. The DUT (amplifier, converter, T/R module) needs to be connected only once to provide full device characterization, including quantities such as conversion gain/loss, intermodulation distortion, compression and group delay.

Straightforward main GUI for amplifier and mixer test setups

The GUI shows the hardware components in the measurement path as graphic elements and helps users optimally configure all the details. Users can see all relevant settings at a glance, including source power, step attenuators, the resulting power level at the reference plane, the internal/external preamplifier gain on the receiver side, and the test parameters. The GUI also provides elements for configuring frequency-converting measurements on mixers and converters; even measurements on high gain receivers with embedded LO can be easily configured and deliver reliable results.

Calibration features and settings

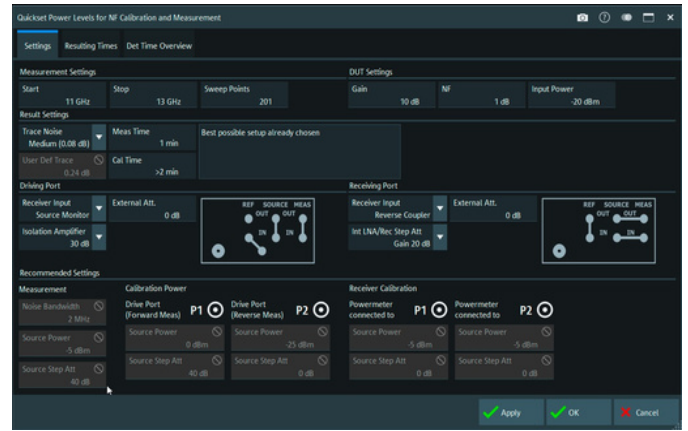
The challenge many instruments and devices are facing with this type of measurement is to handle very low stimulus powers and high measured power levels that may even differ for calibration and measurement and in the forward and reverse direction. The main GUI includes essential parameters to help users easily find the desired settings with manual configuration. Correction algorithms such as used in system error correction provide accurate and reliable results.



GUI for configuring noise figure measurements on amplifiers, mixers, converters and T/R modules

Quickset—the fast and intuitive way to optimal settings

As an alternative to direct manual configuration of measurement and calibration parameters and the R&S®ZNA hardware, the extremely powerful Quickset dialog guides users interactively to the optimal setup. Based on estimated DUT characteristics such as the approximate noise figure (NF) and gain and the desired noise figure accuracy, the R&S®ZNA calculates parameters such as the measurement time and source power and displays the recommended optimal hardware configuration (e.g. use of direct source monitor access, low-noise preamplifier at receiver port 2 or reverse coupler operation). Interactive graphic elements help the user modify settings. The effects of modifications are calculated and displayed instantaneously and can be assessed by the user. This is a quick way to configure reliable noise figure measurements on amplifiers.



Quickset dialog for interactive and semi-automatic configuration of optimal test parameters and R&S®ZNA hardware

Options supporting noise figure measurements

| Designation | Type | Required/recommended | Comment |
|--|---|--|---|
| Noise figure measurements | R&S®ZNA-K30 | required | with R&S®ZNA-K4: support of frequency-converting measurements |
| Options for source port 1 (port 3) configuration | | | |
| Direct source monitor access, port 1/port 1 and port 3 | R&S®ZNAxx-B161/ R&S®ZNAxx-B163 ¹⁾ | required | provides a relatively strong reference signal with very low stimulus powers, for low trace noise (requires R&S®ZNAxx-B16/-B21/-B23) |
| Source step attenuator, port 1/port 3 | R&S®ZNAxx-B21/ R&S®ZNAxx-B23 | required with R&S®ZNAxx-B161/-B163, step attenuator for port 1 | variation of source power, for two-tone signals, attenuators at both source ports P1 and P3 are recommended |
| Receiver step attenuator, port 1 | R&S®ZNAxx-B31 | required | power level optimization at measurement receiver |
| Low-power spurious reduction, port 1 | R&S®ZNAxx-B501/ R&S®ZNAxx-B511 | recommended | recommended with high gain DUTs (requires R&S®ZNAxx-B31; recommended: R&S®ZNAxx-B21/-B23, R&S®ZNAxx-B16, R&S®ZNAxx-B161/-163) |
| Options for receiver port 2 configuration | | | |
| Low-noise preamplifier, port 2 | R&S®ZNAxx-B302/ R&S®ZNAxx-B312 | strongly recommended | switchable internal preamplifier, selectable gain steps (requires R&S®ZNAxx-B16, R&S®ZNAxx-B32) |
| Receiver step attenuator, port 2 | R&S®ZNAxx-B32 | strongly recommended, required with R&S®ZNAxx-B302/-B312 | power level optimization at measurement receiver |
| Direct source and receiver access | R&S®ZNAxx-B16 | recommended, required with R&S®ZNAxx-B302/-B312 | supports reversed coupler operation for increased receiver sensitivity |

¹⁾ xx designates the R&S®ZNA model.

PULSED MEASUREMENTS – FAST AND SIMPLE

The R&S®ZNA offers pulse modulators, pulse generators and synchronization I/Os for analyzing active components under pulsed conditions. Typical DUTs include components and complete T/R modules for radar applications. S-parameters, input and output powers and intermodulation products can be measured without any external components to generate RF pulses and synchronize test sequences.

Internal pulse modulators and pulse generators

The R&S®ZNA can be equipped with one pulse modulator (R&S®ZNAxx-B4n) per port. The pulse modulators can be controlled via external pulse sources or via the four internal pulse generators. The internal pulse generators can also be used to control external pulse modulators via the trigger board outputs. This allows special modulators for very short pulses to be integrated, for example.

Thanks to the test set architecture, once system error calibration has been performed, it remains valid for all types of pulsed measurements – versus frequency, power and time – even if the pulse duty cycle is changed. The R&S®ZNA digital section is designed so that users can configure the pulse parameters individually for each port, supported by a convenient GUI. In addition to double pulses, users can configure arbitrary pulse sequences (i.e. with arbitrary start and stop times for all pulses) in a clearly laid out table.

Measurements versus frequency and power

The R&S®ZNA supports the common measurement techniques for pulsed applications such as point-in-pulse and pulse profile measurements. For average pulse measurements, which rely on narrow IF bandwidths, the R&S®ZNA offers highly selective IF digital filters for the carrier signal.

Point-in-pulse measurements

Short sampling times of 32 ns are achieved for point-in-pulse measurements with IF bandwidths ranging up to 30 MHz. In addition to S-parameters, the absolute peak power can be determined in amplitude and intermodulation measurements. Flexible trigger functions support complex pulsed measurement scenarios and facilitate synchronization of measurements.

Pulse profile analysis versus time with 8 ns resolution

Equipped with the R&S®ZNA-K7 option (measurements on pulsed signals), the R&S®ZNA supports pulse profile measurements with a time resolution of 8 ns. This technique is suitable for periodic, non-periodic and one-shot pulse scenarios.

The analyzer provides simultaneous measurement of a signal on multiple receivers and for multiple wave quantities. The maximum number of wave quantities depends on the IF bandwidth and can vary e.g. between two (at 30 MHz IF bandwidth) and eight (at 1 MHz IF bandwidth). The number of wave quantities can be doubled using the R&S®ZNA-B7 data streaming memory option.

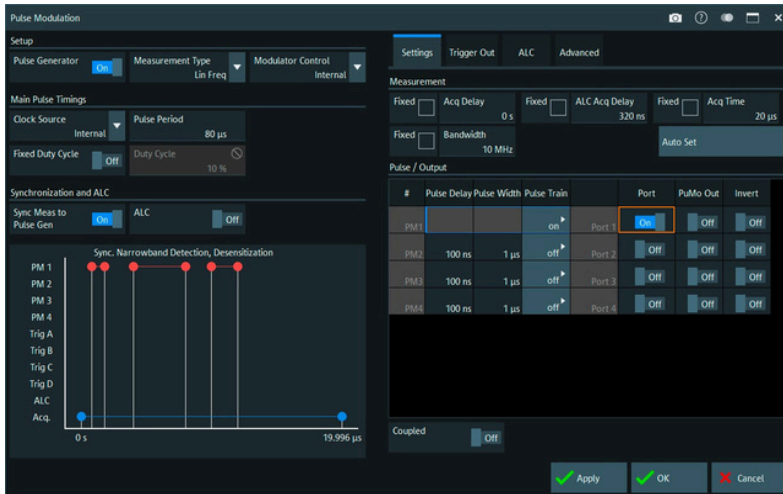
Pulsed measurements

| | Functions | Options |
|-----------------------------|---|---|
| Hardware | <ul style="list-style-type: none"> ▶ Four internal pulse generators with 4 ns time resolution and 8 ns minimum pulse width ▶ One pulse modulator per port with 40 ns minimum pulse width ▶ Four trigger inputs ▶ Four trigger outputs | <p>The internal pulse generators are enabled with one of the following options: R&S®ZNA-B91 (trigger and control I/O board) or R&S®ZNAxx-B4n (internal pulse modulator, port n).</p> <p>The R&S®ZNA-B7 (data streaming memory) increases the number of wave quantities that can be measured in parallel with the R&S®ZNA-K7 (measurements on pulsed signals).</p> |
| Pulse profile measurements | <ul style="list-style-type: none"> ▶ Up to 30 MHz IF bandwidth ▶ 8 ns time resolution ▶ 40 ns minimum pulse width | R&S®ZNA-K7 (measurements on pulsed signals) |
| Point-in-pulse measurements | 40 ns minimum pulse width (30 MHz IF bandwidth) | R&S®ZNA-K17 (increased IF bandwidth 30 MHz) |

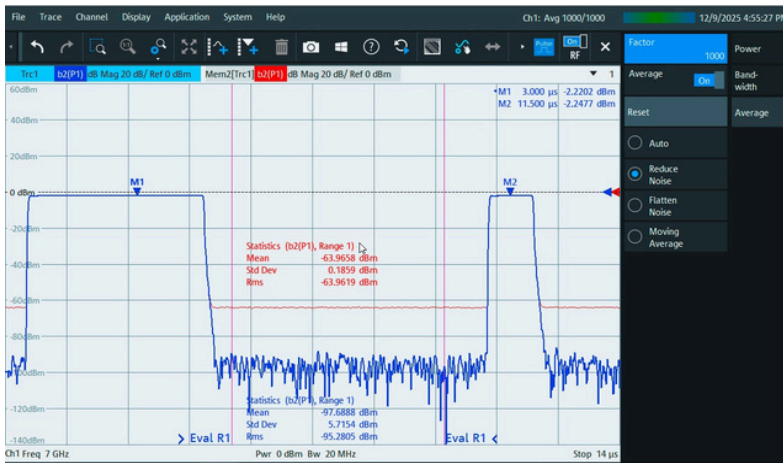
Wideband pulsed measurements with high dynamic range

With up to 30 MHz IF bandwidth, the R&S®ZNA provides point-in-pulse and pulse profile measurements on very short pulses. At the same time, the analyzer offers techniques to deliver extremely low-noise traces or achieve a very high dynamic range despite the wide measurement bandwidth.

Unique in the R&S®ZNA is a method for averaging complex values, which allows sensitivity in the order of -90 dBm to be achieved at an IF bandwidth of 10 MHz, for example.



Configuration of parameters for pulsed signal measurements



Pulse profile measurement: the wideband measurement mode enables single-shot pulse sweeps without averaging. Averaging (AVG) modes are also available to achieve either a very low trace noise or a very high dynamic range (i.e. a high pulse on/off ratio) based on vector averaging. Red trace: AVG mode "flatten noise". Blue trace: AVG mode "reduce noise".



Pulse profile measurement with arbitrary pulse sequences. Pulse sequences can be measured on multiple receivers simultaneously. Since the receivers are phase coherent, they not only measure the amplitude of a pulse but also its phase with high stability. This allows the phase deviation of a DUT to be determined very simply and reliably.

MIXER MEASUREMENTS EASIER THAN EVER

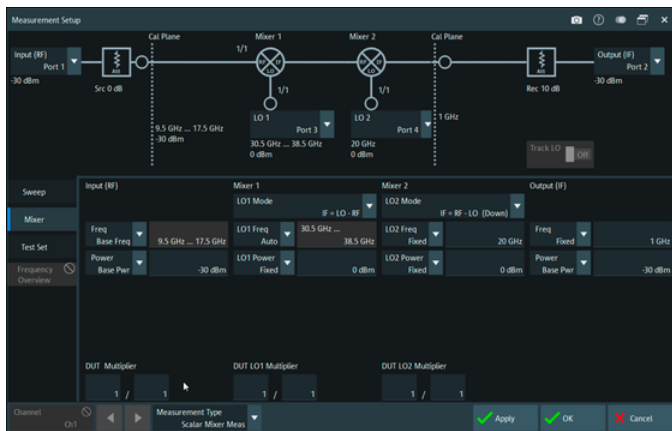
System error corrected mixer phase and group delay tests with up to four sources for I Mon mixers and double converting receivers

Fast setup and short measurement times with four internal sources and two internal LOs

The R&S®ZNA 4-port model comes with up to four internal sources. Swept LO measurements and intermodulation measurements versus frequency on mixers are performed up to ten times faster compared to setups that use

external sources. With separate sources independently configurable by port, even double-converting receivers can be characterized with the R&S®ZNA single box solution with unrestricted configuration flexibility and optimum accuracy. In addition, the rear panel local oscillator (LO) output is available as a scalar LO source up to 26.5 GHz.¹⁾ With two independent LOs for the internal receivers, the R&S®ZNA can perform simultaneous RF/IF measurements on mixers at twice the speed of a single LO while reducing trace noise during conversion loss and group delay measurements.

DUT-centric configuration of mixer measurements

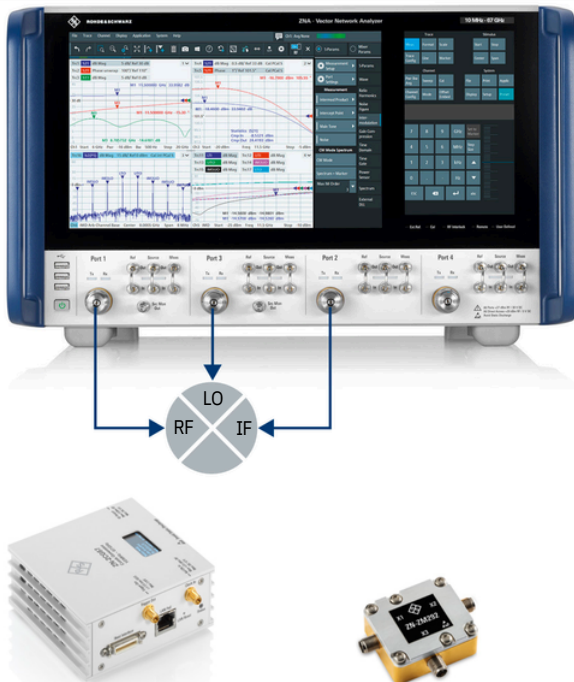


High accuracy and easy configuration thanks to R&S®SMARTerCal

The R&S®ZNA determines the return loss and conversion loss of mixers and converters with high precision using R&S®SMARTerCal, a special calibration technique that combines system error correction with absolute power level calibration. It corrects mismatch of the test ports and

¹⁾ Requires R&S®ZNA-B8 and ZNAXx-B5 options.

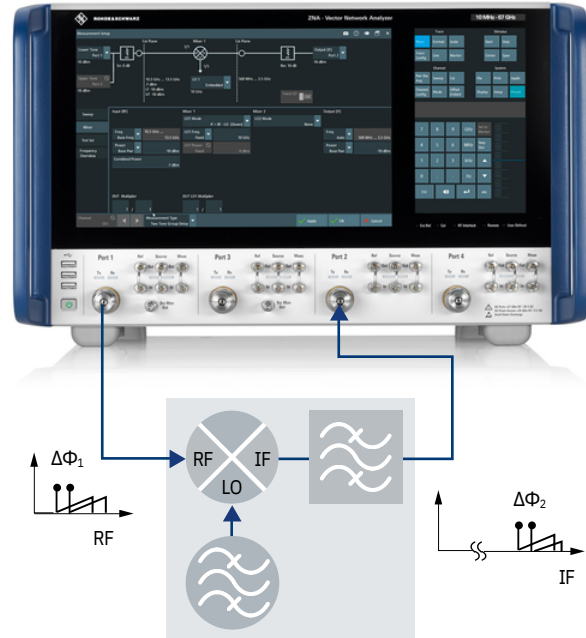
Phase measurement on a mixer



R&S®ZN-CZG as phase reference

R&S®ZN-ZM292 calibration mixer

Group delay measurement on a converter with two-tone signal applied to the mixer

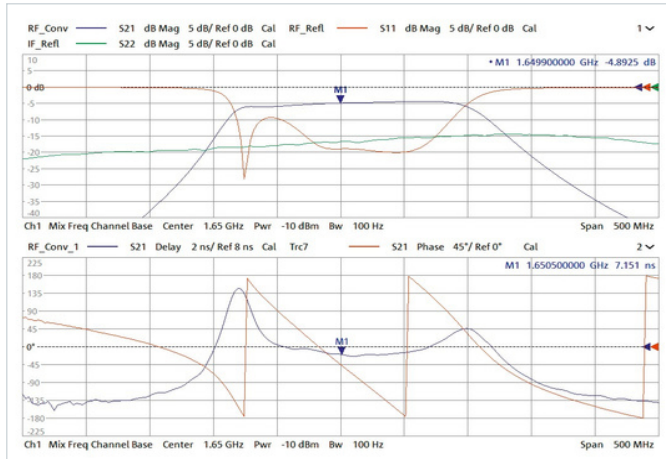


Two-tone signal obtained with R&S®ZNAXx-B213 internal combiner or an external combiner

mixer; no attenuators are needed to improve port matching. Port match correction also ensures accurate results when using the R&S®ZNA-K9 option (group delay measurements on frequency converters without LO access).

Unique approach for phase and group delay measurements on converters without LO access

The R&S®ZNA offers a special technique for measuring group delay and relative phase on frequency converters in cases where there is no access to the internal LO or the reference frequency. The analyzer uses a two-tone signal to stimulate the DUT. From the phase difference between the carriers at the input and output, the instrument calculates the group delay and the relative phase. The frequency



drift and frequency modulation of the DUT's internal LO do not affect the measurement accuracy as long as the frequency deviation lies within the analyzer's IF bandwidth used for the measurement.

Phase measurements on frequency converters using vector error correction

Any receiving system requires a flat amplitude and phase response in order to transmit information smoothly and without disruptions. With the R&S®ZNA-K5 option (vector corrected converter measurements), the R&S®ZNA determines the magnitude and phase for the transmission parameters of mixers and converters with LO access. This measurement uses the phase coherent, phase repeatable synthesizers in the R&S®ZNA in combination with a 2-port power UOSM (PUOSM) calibration. The measurement itself does not require a reference mixer for frequency back-conversion. However, using a mixer for calibration can potentially compromise the accuracy because of non-reciprocity and the band-limited usable frequency range. Using the R&S®ZN-ZCG comb generator as a phase reference is a more versatile and unambiguous solution. The measurement is quick and easy to configure. It delivers the magnitude and phase for all four system error corrected S-parameters of a frequency converter, as well as its phase and group delay and AM/AM and AM/PM conversion.

Results of a converter measurement including return loss, conversion loss, phase and group delay

Frequency-converting measurements

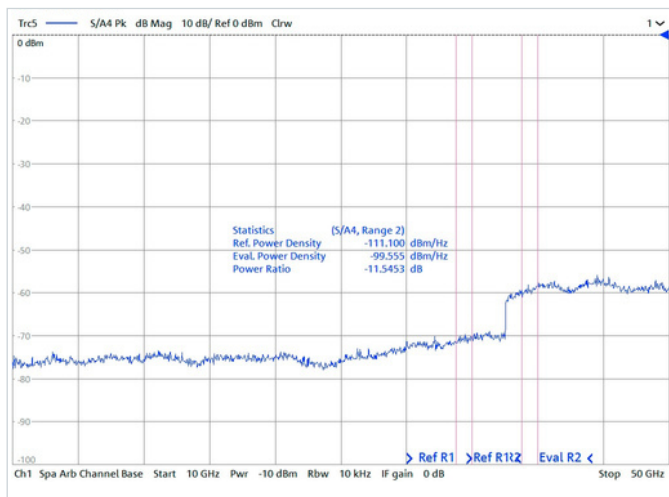
| Type of measurement | Functions | Options |
|--|---|---------------------------|
| Scalar mixer and arbitrary frequency-converting measurements | <ul style="list-style-type: none"> ▶ Conversion loss of mixers ▶ 2nd source for swept LO measurements ▶ 3rd and 4th internal source for intermodulation measurements on mixers and receivers with two converter stages ▶ R&S®SMARTerCal for vector error corrected scalar frequency-converting measurements ▶ Correction of mismatch on test ports ▶ Scalar conversion loss and return loss ▶ Isolation measurement: LO → RF and LO → IF ▶ Intermodulation products and nth-order intercept point ▶ AM/AM conversion | R&S®ZNA-K4, R&S®ZNAxx-B3n |
| | <ul style="list-style-type: none"> ▶ 2nd internal LO source for twice the measurement speed ▶ Rear panel output for internal LO signal as the 5th source (when 2nd internal LO source (R&S®ZNA-B5, up to 26.5 GHz) is installed, the 2nd LO source is made available at the output) | R&S®ZNA-B5, R&S®ZNA-B8 |
| Vector error corrected converter measurements | <ul style="list-style-type: none"> ▶ 2-port power UOSM (PUOSM) calibration for vector error corrected conversion loss measurements ▶ Forward and reverse conversion loss (magnitude and phase) ▶ Absolute/relative group delay ▶ AM/AM and AM/PM conversion | R&S®ZNA-K5 |
| | <ul style="list-style-type: none"> ▶ Calibration mixer | R&S®ZN-ZM292 |
| Measurements on frequency converters without LO access | <ul style="list-style-type: none"> ▶ Group delay and relative phase ▶ 2nd internal LO for twice the measurement speed and for low trace noise | R&S®ZNA-K9, R&S®ZNA-B5 |

SPECTRUM ANALYSIS WITH MULTI CHANNEL VIEW

The R&S®ZNA-K1 spectrum analysis function provides a deeper insight into a DUT's behavior where S-parameter measurements versus frequency and power are not sufficient.

The FFT-based spectrum analysis function can be used to measure a DUT's spurious and harmonics, providing short sweep times along with high dynamic range and fine frequency resolution. It quickly detects undesired signal components (spurious) in converters and T/R modules. The marker-to-spectrum function directly gets to the root of problems in the event of unexpected S-parameter results, thus providing fast and extremely useful integrated diagnostics.

R&S®ZNA-K1 analysis functions: display of the ratio of power densities from different segments and the noise power marker function



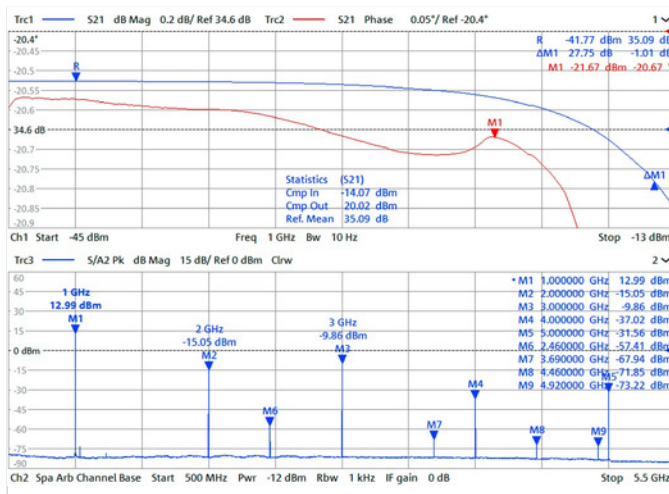
Multichannel view of mixer measurements with harmonic and spurious search

The spectrum analysis function is available on all ports of the R&S®ZNA. It relies on system error correction (OSM port match correction), boosting accuracy and eliminating the influences of the test setup. In multichannel view, multiple results are displayed simultaneously. For example, an S-parameter measurement can be displayed along with the harmonics spectrum, or the conversion loss along with the spurious signals for a mixer. The R&S®ZNA-K1 spectrum analysis results can be displayed from all measurement and reference receivers in one setup. True parallel detection and display of the results from up to four receivers significantly reduces test time.

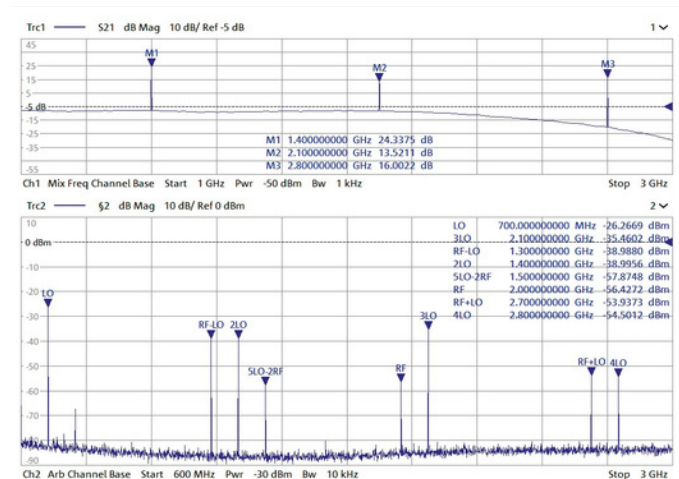
Combined S-parameter and spectrum analysis with marker function

When undesired effects are detected during S-parameter measurements, the root cause of the problem can be identified with a subsequent spectrum analysis, which is performed at the press of a button. A marker is placed on the desired frequency, and spectrum analysis around this frequency will deliver conclusive information about unwanted effects. In addition, a noise marker can be used to display the normalized noise power in dBm (1 Hz).

R&S®ZNA-K1 spectrum analyzer option: amplifier magnitude and phase compression measurement (at 1 GHz, top) and corresponding harmonic and spurious spectrum



R&S®ZNA-K1 spectrum analyzer option: output spectrum of a mixer



TIME DOMAIN ANALYSIS AND SIGNAL INTEGRITY MEASUREMENTS

The R&S®ZNA-K2 and R&S®ZNA-K20 options provide a wide range of features for in-depth investigation of transmission line structures, signal transmission quality and in-fixture/PCB testing.

Efficient time domain analysis with enhanced resolution

The R&S®ZNA offers powerful time domain analysis to measure components such as test fixtures, cables and connectors in the frequency and time domain. With up to 100 000 points per trace, the R&S®ZNA can easily measure even electrically long DUTs such as cables. Using the gating function, the analyzer can locate discontinuities and analyze them in detail.

A 4-port R&S®ZNA can be used to determine the balanced S-parameters and other quantities such as near-end and far-end crosstalk (NEXT, FEXT) on two-wire lines and differential structures. Using the Rohde & Schwarz VNA unique resolution enhancement function, the frequency range of the R&S®ZNA can be virtually extended. This yields temporal and spatial resolution substantially higher than would be expected from the DUT's and/or analyzer's frequency range.

Distance-to-fault measurements

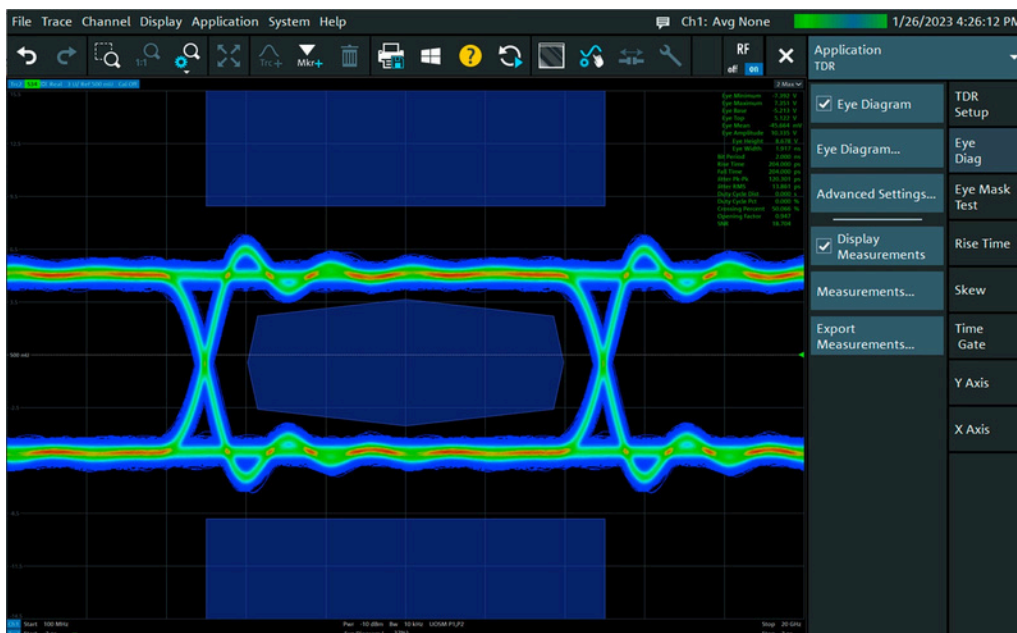
The R&S®ZNA-K2 time domain analysis option has a special menu for the straightforward configuration of distance-to-fault (DTF) measurements. Discontinuities in transmission lines are directly measured and displayed versus distance using S-parameter reflection measurements.

Signal integrity at a glance with eye diagrams

Verifying the quality of a transmission path usually requires testing all of its components. The R&S®ZNA provides comprehensive analysis of cables and connectors in the time and frequency domain. The R&S®ZNA-K20 extended time domain analysis option makes it possible to compute, based on the S-parameters, the rise time, skew and eye diagrams for different bit patterns. The R&S®ZNA-K2 time domain analysis and R&S®ZNA-K20 extended time domain analysis options are integrated into the analyzer firmware. Eye diagrams and S-parameters versus frequency and time can be analyzed and displayed simultaneously, revealing the transmission quality at a glance.

Analysis of disturbance effects and signal quality optimization

The R&S®ZNA-K20 extended time domain analysis option makes it possible to simulate the effects of disturbances such as jitter and noise on the eye diagram. The analyzer can also simulate the impact of correction algorithms, e.g. for predistortion at the transmitter end and for equalization at the receiver end. Plus, the R&S®ZNA-K20 option can be used to configure user-defined mask tests. These tests make it possible to verify compliance of the DUT's behavior with relevant standards such as USB, HDMI™ and DVI.



The R&S®ZNA-K20 option offers versatile signal integrity measurements, e.g. eye diagrams with a mask to verify compliance with relevant requirements. It can also be used to determine the transmission characteristics of signals with jitter or noise.

PHASE-CONTROLLED SOURCE MEASUREMENTS

Phase control of up to eight digital RF sources enables multi-path propagation evaluation, phased antenna array/TRM testing, I/Q measurements, and fully automated true differential mode testing.

Innovative digital LO and RF synthesizers

Thanks to R&S®ZNA digital (DAC based) synthesizers, sources can be set to dedicated phase values. This concept is the basis for well defined stimulus phase conditions in the reference planes, and unambiguous synchronous phase measurements even with the receivers at different frequencies.

A variety of advanced measurements is supported:

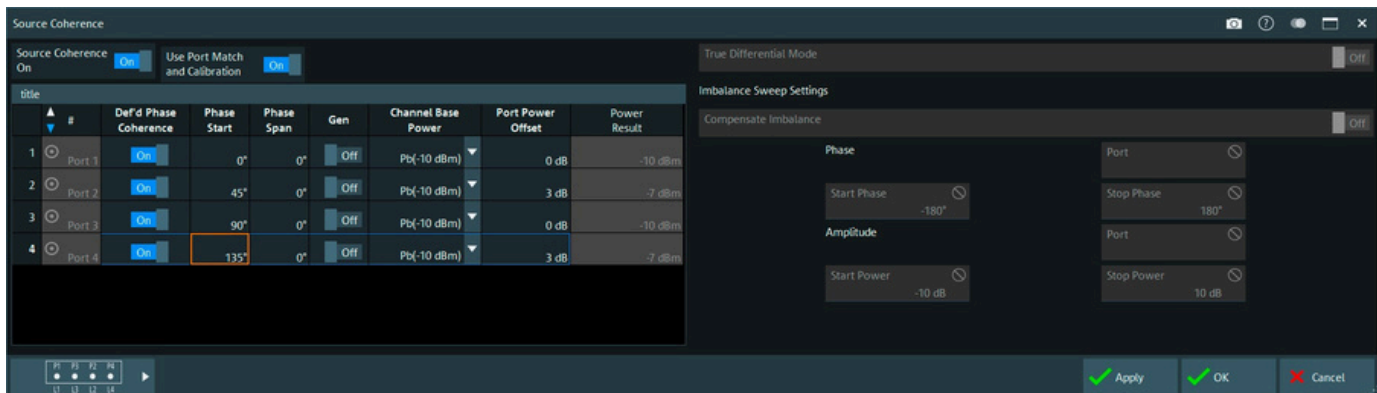
- ▶ Arbitrary phase source setting for I/Q applications
- ▶ Testing differential amplifiers under real operating conditions
- ▶ Evaluation of the phase and magnitude imbalance of balanced and multipath systems
- ▶ Tuning the radiation pattern of antenna arrays and subarrays (AESA)
- ▶ Phase tuning of all RF sources allows amplifier active load pull tests
- ▶ Getting differential or mixed-mode S-parameters of differential structures with true-mode stimulation

R&S®ZNA-K6 source-coherent mode

The R&S®ZNA-K6 option enables the phase-coherent operation of the R&S®ZNA sources. Depending on the operation mode, arbitrary phase state values can be entered for each source as required. Full n-port and level calibration ensure high-phase and level accuracy in the reference plane and minimum phase uncertainty by port match correction.

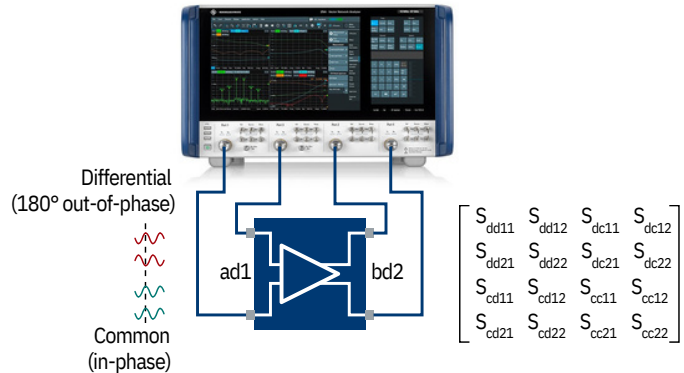
GUI for entering dedicated port specific values for phase and power.

In automatic true differential measurement mode, users can enter parameters for phase and magnitude imbalance sweeps.



True differential test mode

The true differential test mode benefits from the source-coherence capability of the RF sources. Alternating stimulus with two 0° in-phase and 180° out-of-phase signals provides all elements of the complete mixed mode S-parameter matrix.



R&S®ZNA-K61 true differential mode testing

Differential amplifiers may respond differently depending on whether they are tested with sequential single-ended or true differential mode stimulation. The use of baluns involves severe limitations: no common mode or mode conversion evaluation, band limitation, limited phase symmetry. R&S®ZNA-K61 overcomes this issue, with true-mode stimulation, and fully automated test execution, applying true common and differential signals, measuring the DUT response. As a result, all elements of the mixed-mode S-parameter matrix are available. In addition, imbalance sweeps for the phase (phase sweep at fixed frequency and power) or magnitude (magnitude sweep at fixed frequency and phase) are supported.



Balanced structures as well as used and unused ports are defined at a keystroke. Predefined topologies are completed with a tab offering free user configurations.

Definition of differential structures at a keystroke

To define the balanced structure and balanced/single-ended ports of the DUT, a clear GUI allows to select the desired topology from predefined settings at a keystroke. Additional configurations are done in just a few mouse clicks.

Application: differential I/Q test

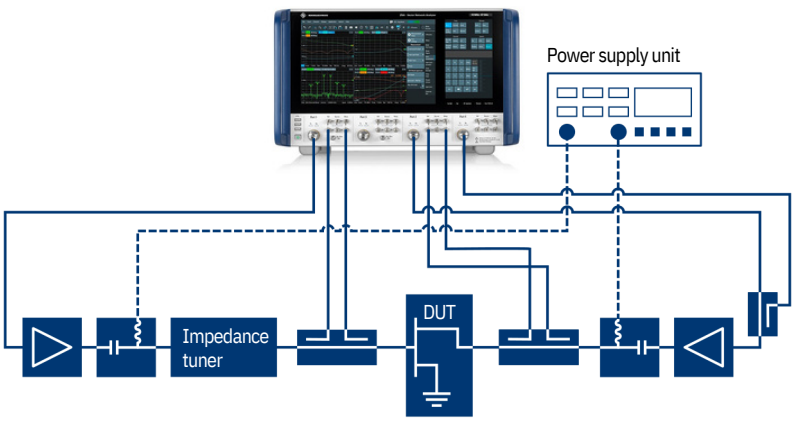
With up to four phase coherent sources, devices with I/Q input/output can flexibly be characterized. The sources can be set to arbitrary phase and magnitude values, to apply 90°/180° I/Q signals, or to perform imbalanced sweeps.

Application: active load pull

Tuning the magnitude and phase of all sources makes it possible to electronically tune the source at the amplifier output in parallel to the RF stimulation. This enables electronic output impedance tuning (reflection coefficient at the amplifier output). Fast tuning lets users evaluate amplifier gain, matching and efficiency in a short test time. Combining the R&S®ZNA with systems from partner companies enables even more comprehensive characterization based on hybrid load pull tuning, e.g. for noise parameter tests.

R&S®ZNA based source/load pull system

The multiple source concept of the R&S®ZNA supports the RF signal plus DUT reverse stimulation and active impedance tuning, offering active source/load pull testing in a compact single-box solution.



APPLICATIONS



PASSIVE DEVICE CHARACTERIZATION

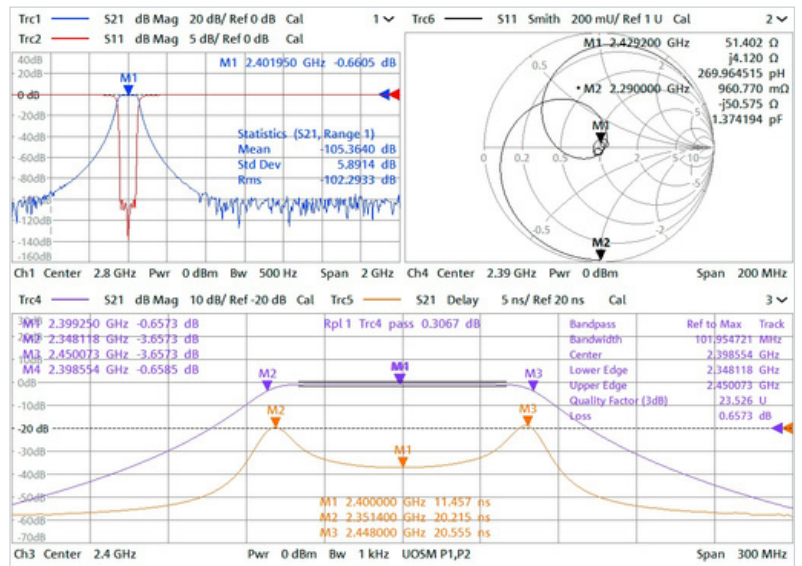
With an exceptional dynamic range and versatile measurement and analysis features the R&S®ZNA is prepared for the characterization of challenging passive devices.

The task

Even passive device characterization may require a wide feature set and challenging instrument specifications:

- ▶ Get maximum throughput in production
- ▶ Minimize sweep time by finding the golden optimum between accuracy and sweep speed
- ▶ Short measurement times despite high dynamic range
- ▶ Comprehensive online analysis, pass/fail
- ▶ Measurement system and handler synchronization

The online analysis functions of the R&S®ZNA enable comprehensive DUT certification without external data analysis. Preloaded setups are represented by tabs and setup swap is done at the click of a mouse. Distributed over several screens (setups), a multitude of results is clearly displayed, and the R&S®ZNA is quickly ready for a new DUT.



| On | Start | Stop | Freq Step Size | Points | Bandwidth | Segm Time | Auto |
|-------------------------------------|----------|----------|----------------|--------|-----------|-----------|-------------------------------------|
| <input checked="" type="checkbox"/> | 1.4 GHz | 2.33 GHz | 2.325 MHz | 401 | 100 Hz | 4.17 s | <input checked="" type="checkbox"/> |
| <input checked="" type="checkbox"/> | 2.33 GHz | 2.45 GHz | 600 kHz | 201 | 1 kHz | 214.34 ms | <input checked="" type="checkbox"/> |
| <input checked="" type="checkbox"/> | 2.45 GHz | 3.4 GHz | 2.375 MHz | 401 | 100 Hz | 4.17 s | <input checked="" type="checkbox"/> |

Buttons: + Add, - Delete, Import, Show Point List, + Insert, - Delete All, Export, Active Segment Settings, OK, Cancel

The segmented sweep allows definition of different test parameters for subsegments of a sweep, e.g. high power and narrow IFBW in the stop band of a filter for high dynamic, and a wider IFBW and narrow frequency grid for short test time and high resolution in the pass band.

R&S®ZNA benefits for passive device characterization with challenging DUTs

Function/feature

Up to 170 dB dynamic range ¹⁾

Segmented sweep (number of points, power, IFBW, other, for subsegments of a sweep)

Filter/marker online analysis, limit lines/ripple test

Multiple parallel preloaded setups

Speed improvement (R&S®ZNA-K66 option)

Benefits

Provides high accuracy even with high-blocking filters

Ensures the optimum balance of accuracy, test time, and RF performance depending on the DUT properties

Offers a comprehensive evaluation and certification of the DUT

- ▶ Reconfigure the measurement task at a mouse click, no time-consuming setup reload required
- ▶ Smart control and clear display of numerous measurement parameters, even for multiple DUTs

Significantly faster group delay measurements for multiband passive component testing with large point counts

¹⁾ Applies in the lower frequency range, options required, data confidence level: "measured".

HIGH-POWER AMPLIFIER AND LNA TESTING

The R&S®ZNA enables high-power amplifier and LNA testing under real operating conditions.

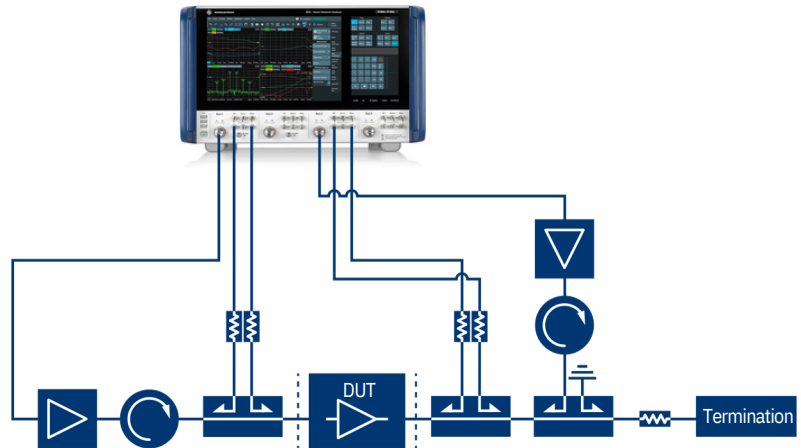
The task

The variety of test parameters and test setups for amplifier characterization calls for a wide range of personalities and configuration flexibility of the test equipment:

- ▶ Handling of very high power levels, external high-power test setups
- ▶ Ensuring stable and drift-independent power levels
- ▶ Multiple tones for intermodulation tests, even on mixers
- ▶ Measurements under pulsed conditions
- ▶ Active device with differential structures
- ▶ Evaluation of noise figure and noise parameters of unmatched DUTs under variable matching conditions

Direct channel access option

With the direct channel access option, as well as source and receiver step attenuators, the R&S®ZNA supports external high-power test setups (with external preamplifier in forward and reverse directions, high-power couplers, attenuators and circulators)



R&S®ZNA benefits for high-power amplifier and LNA testing

Function/feature

Benefits

| | |
|--|--|
| Up to 4 internal, independently configurable sources, internal combiner | Intermodulation testing (without external sources) at full speed and configuration flexibility, even in combination with mixers |
| Unique power sweep range of 100 dB, attenuators, compression point personality | Compression evaluation over wide power ranges, including real-time compression point (CP) evaluation |
| Combination of sweep modes | Magnitude and frequency offset swept measurements, AM/AM and AM/PM tests |
| Digital automatic level control (ALC), with arbitrary reference signal access | Accurate and stable stimulation power even with external preamplifiers |
| Control of external power supply units | Power added efficiency (PAE) test |
| Four integrated pulse modulators, pulse profile test option | High-power point-in-pulse test, pulse profile analysis |
| True differential mode | Reliable characterization of differential amplifiers without external baluns, mode-conversion parameters and phase/magnitude imbalance sweeps |
| Noise figure personality and preamplifier | Noise figure tests without reconnection and noise source |
| Source phase control, partner system integration (Focus Microwaves and Maury Microwave): active harmonic load pull | <ul style="list-style-type: none"> ▶ On-wafer chip characterization ▶ Impedance tuning for unmatched amplifiers ▶ Active harmonic load pull testing (with electronic and hybrid impedance tuning) |

RECEIVER AND LNB CHARACTERIZATION

The R&S® ZNA enables reliable (high-gain) receiver and LNB characterization with a simple setup.

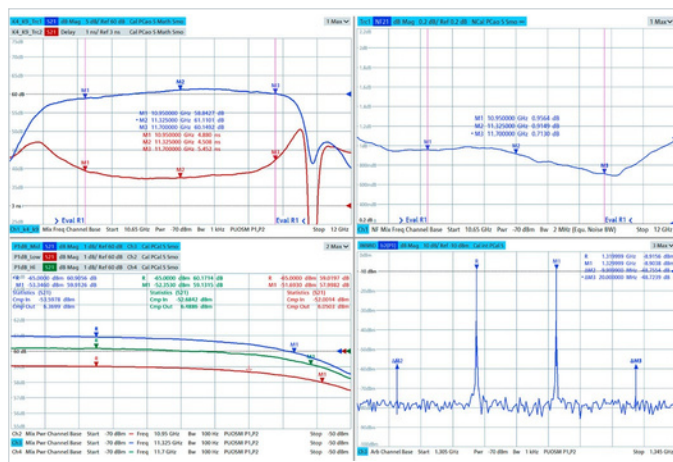
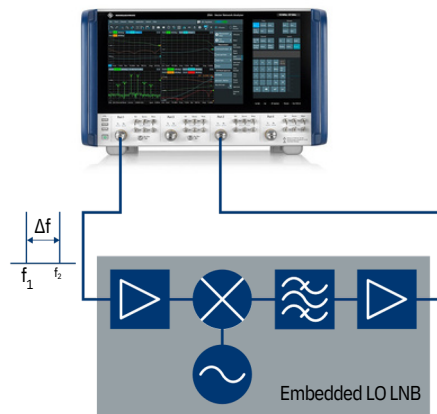
The task

There are several special aspects which make high-gain converter testing challenging:

- ▶ Requirement of several sources for intermodulation test with dual LO devices (with LO access)
- ▶ IF frequency offset from an internal oscillating LO
- ▶ Mixer group delay test without LO access
- ▶ Noise figure test on mixers
- ▶ High accuracy, low traces noise, and short test time despite of very low stimulation power

Embedded LO converter test setup

With dedicated functions, such as LO tracking and two-tone based group delay measurement, R&S® ZNA enables a reliable and comprehensive characterization of frequency converters without access to the internal local oscillator



Example result screen of embedded LO converter testing: conversion gain, group delay, noise figure, compression, intermodulation

R&S® ZNA benefits for receiver and LNB characterization

Function/feature

Up to 4 internal, independently configurable sources, internal combiner

Unique solution for embedded LO converter group delay test (R&S® ZNA-K9) and LO tracking function

Flexible frequency conversion capability and mixer phase measurement option

Selectable reference signal access for the stimulation source signal

Port 1 isolation amplifier

Noise figure test options, combined with mixer test setup

2-port R&S® ZNA with 2 sources and internal combiner

Benefits

Intermodulation testing of converters with (accessible) dual LO conversion

Measure converter group delay (GD) reliable despite of significant DUT LO drift, and without access to the internal LO

Phase measurements on converters, LO crosstalk, etc.

Get a sufficient strong reference signal despite of extremely low stimulation power for low trace noise

Get extremely low spur free stimulation signal

Comprising characterization without reconnection, including noise figure test without a noise source

Get intermodulation, group delay and noise figure (NF) from embedded LO converters with a 2-port R&S® ZNA

T/R MODULE AND RADAR AESA TESTING

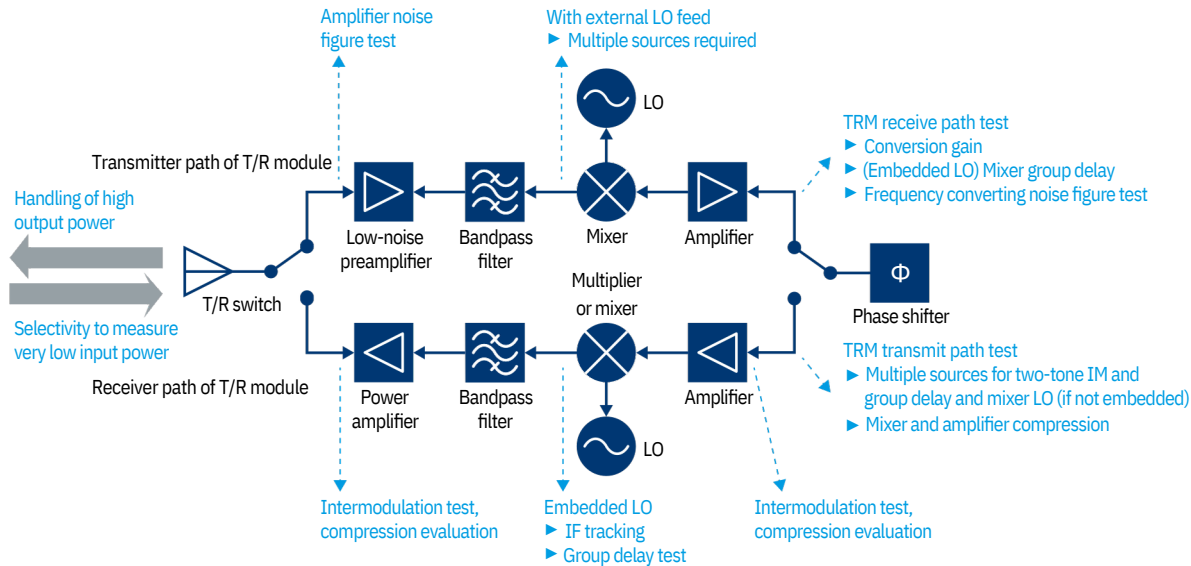
The R&S®ZNA enables comprehensive transmit/receive (T/R) module and radar active electronically scanned array (AESA) testing with a single connection.

The task

T/R modules combine both transmitting and receiving submodules, which requires the following of measurement capabilities:

- ▶ Features for amplifier testing: compression point (CP), intermodulation (IM), noise figure (NF)
- ▶ Handling of very high and very low power
- ▶ Multiple frequency conversion with embedded mixer LO
- ▶ Multiple phase-controlled sources
- ▶ Enhanced DUT control and system support

Typical elements of a radar T/R module, highlighting the challenges for the VNA to characterize single components and the entire module



R&S®ZNA benefits for T/R module and radar AESA testing

Function/feature

Up to 4 internal sources with flexible sweep mode configuration and internal combiner

Phase-coherent source control

Multichannel spectrum analysis option

Enhanced trigger and pulsed I/O

2-port R&S®ZNA with two sources and options for high/low power and noise figure tests

Benefits

- ▶ Receiver intermodulation and compression testing
- ▶ Frequency-converting modules with LO access: support of dual LO design
- ▶ Group delay testing of embedded LO devices

- ▶ Phase measurements on converters
- ▶ Radiation pattern testing with beamforming submodules

Spur search with all R&S®ZNA receivers, effective with up to 4 receivers in parallel

DUT synchronization and control for DUT phase and power settings with synchronized measurement

Comprising characterization of a 2-port T/R module with an R&S®ZNA with two test ports (IM, CP, embedded LO converter group delay)

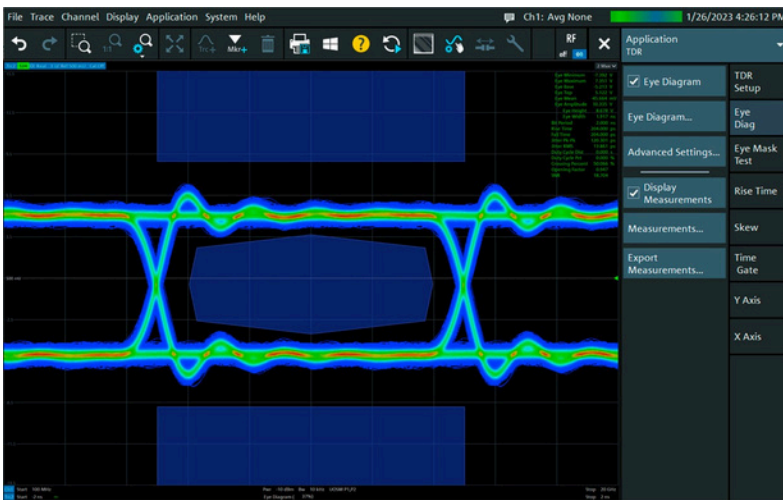
SIGNAL INTEGRITY TESTING

With the enhanced TDR option and deembedding personalities, the R&S®ZNA enables evaluation of the signal transmission quality of lines, cables and PCB structures, including correction techniques for in-fixture, and on-PCB testing.

The task

Increasing data volumes and bit rates demand precise characterization of cables, transmission lines and PCB structures at ever increasing frequency ranges. Simply testing in time and frequency provides reliable characterization, but in-fixture and on-board mounted DUTs call for additional deembedding functionalities:

- ▶ Combination of enhanced time domain analysis results (TDR) and S-parameters
- ▶ In-fixture calibration techniques
- ▶ Techniques for fixture and PCB structure characterization and deembedding
- ▶ Flexible single and multiport configuration



Eye diagram mask test with synthetic signal predistortion

R&S®ZNA benefits for signal integrity testing

Function/feature

Benefits

TDR with various filter and frequency grid configurations, including distance-to-fault test and synthetic frequency extension (R&S®ZNA-K2 option)

- ▶ Optimization of TDR measurement for optimal resolution and band-limited DUTs
- ▶ Easy cable distortion analysis
- ▶ TDR results at a higher resolution than given by DUT band-limitation and the R&S®ZNA frequency range

Enhanced TDR/eye diagram, including bit stream and modulation simulation (R&S®ZNA-K20 option)

Simulated eye diagram analysis for transmission characterization without real pulsed signals

Enhanced in-fixture calibration techniques: TRL/LRL, TNA, TRM, TSM, TOM (R&S®ZNA-K210, -K220, -K230, -K231 options)

Direct in-fixture calibration with custom calibration standards (partially unknown and reduced number of standards)

Enhanced deembedding personalities based on custom tools from partner company

Test coupon based in-fixture and PCB structure characterization including deembedding

SNP assistant (R&S®ZNA-K100 option)

Guided connection steps to derive multi-port S-parameter (.snp) files with a 2-port or 4-port VNA

Speed improvement (R&S®ZNA-K66 option)

Fast sweep mode shortens measurement time, increasing production throughput and enabling full characterization of high-port-count DUTs without compromising accuracy

ANTENNA MEASUREMENTS— THE PERFECT FIT

With its wider range of hardware and software functions, the R&S® ZNA can be used as the high-performing core in near-field, far-field, compact range and radar cross section (RCS) antenna test systems.

Fast antenna characterization

The outstanding receiver sensitivity of the R&S® ZNA, in combination with fast synthesizers, speeds up antenna characterization even when measuring very low signal levels. The analyzer's high sensitivity, low trace noise, wide range of selectable IF bandwidths and various averaging functions help to find the optimum balance of short test times and high accuracy.

For test systems employing external mixers, the R&S® ZNA allows flexible, independent configuration of the frequencies and powers for all sources and receivers, as well as direct IF signal path access with selectable IF frequencies.

Measurements on antenna arrays

The R&S® ZNA can provide stimulus signals from up to four sources, making it possible to measure the directional pattern of electronically controlled antenna arrays. In addition, the internal LO signal (standard LO or second internal LO source up to 26.5 GHz) is accessible on the rear panel. This means that up to five sources are available for feeding antenna arrays or for external up/down conversion.

Featuring a truly parallel receiver architecture with up to eight receivers, the analyzer reliably measures the amplitude and phase of up to eight input signals. The R&S® ZNA can therefore be used as a compact multi-channel receiver to design antenna arrays and sub-arrays for MIMO mobile communications systems, or it can be used as part of antenna test systems employing horizontally and/or vertically polarized antennas as well as reference receiving antennas.

R&S® ZNA benefits for antenna measurements

| Function/feature | Benefits |
|---|--|
| High receiver sensitivity up to -151 dBm (1 Hz) (typ., with direct receiver access) | Short measurement times |
| Inputs for direct access to IF signal paths, selectable IF frequencies with 1 GHz bandwidth | Use in high-frequency test systems with external mixers Adaptation to optimal IF of test system |
| Identical RF design of all receivers | Identical characteristics of measurement and reference channels |
| Up to 5 internal sources ¹⁾ | <ul style="list-style-type: none"> ▶ Multi-antenna stimulation ▶ LO signals for external mixers |
| Configuration of arbitrary frequency-converting measurements | Universal support for external mixers and mmWave systems |
| Reverse frequency sweep | <ul style="list-style-type: none"> ▶ Alternating movement of positioner (CW, CCW in azimuth, as well as movement in elevation) ▶ Spherical near-field measurements |
| Extended trigger functionality | <ul style="list-style-type: none"> ▶ Optimal synchronization of positioner, clock generators, etc. ▶ Simple and flexible system integration |
| Truly parallel receiver architecture | <ul style="list-style-type: none"> ▶ Measurements with up to eight receivers (no multiplexing) ▶ Simultaneous measurements of multiple antenna polarizations (horizontal/vertical) and antenna arrays (MIMO) |
| mmWave converters | Measurements in mmWave range |

¹⁾ Up to four RF sources plus LO source (on rear panel output, 2nd internal LO source up to 26.5 GHz).

RCS measurements and measurements on complete RX modules

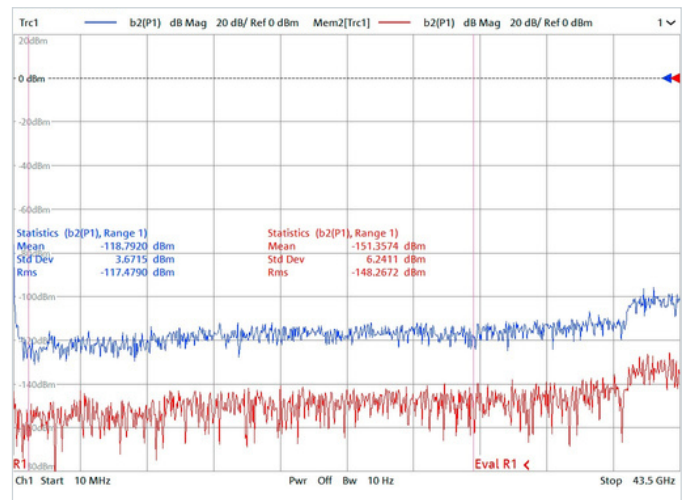
The R&S®ZNA can perform RCS measurements and measurements on complete RX modules without any external test equipment. With up to four signal sources, up to four internal pulse modulators and generators, up to eight true receivers, and the ability to sample up to 16 wave quantities in parallel, the R&S®ZNA provides signal generation and multichannel measurements in a single, compact platform (see also "Pulsed measurements – fast and simple", page 38).

Data streaming mode

The R&S®ZNA-K28 data streaming mode option allows continuous sweep recording and writing to a circular buffer. The controlled timing feature ensures constant measurement times for every sweep point and gapless recording. Thus, the user-defined number of sweeps and traces is merged to one common data set.

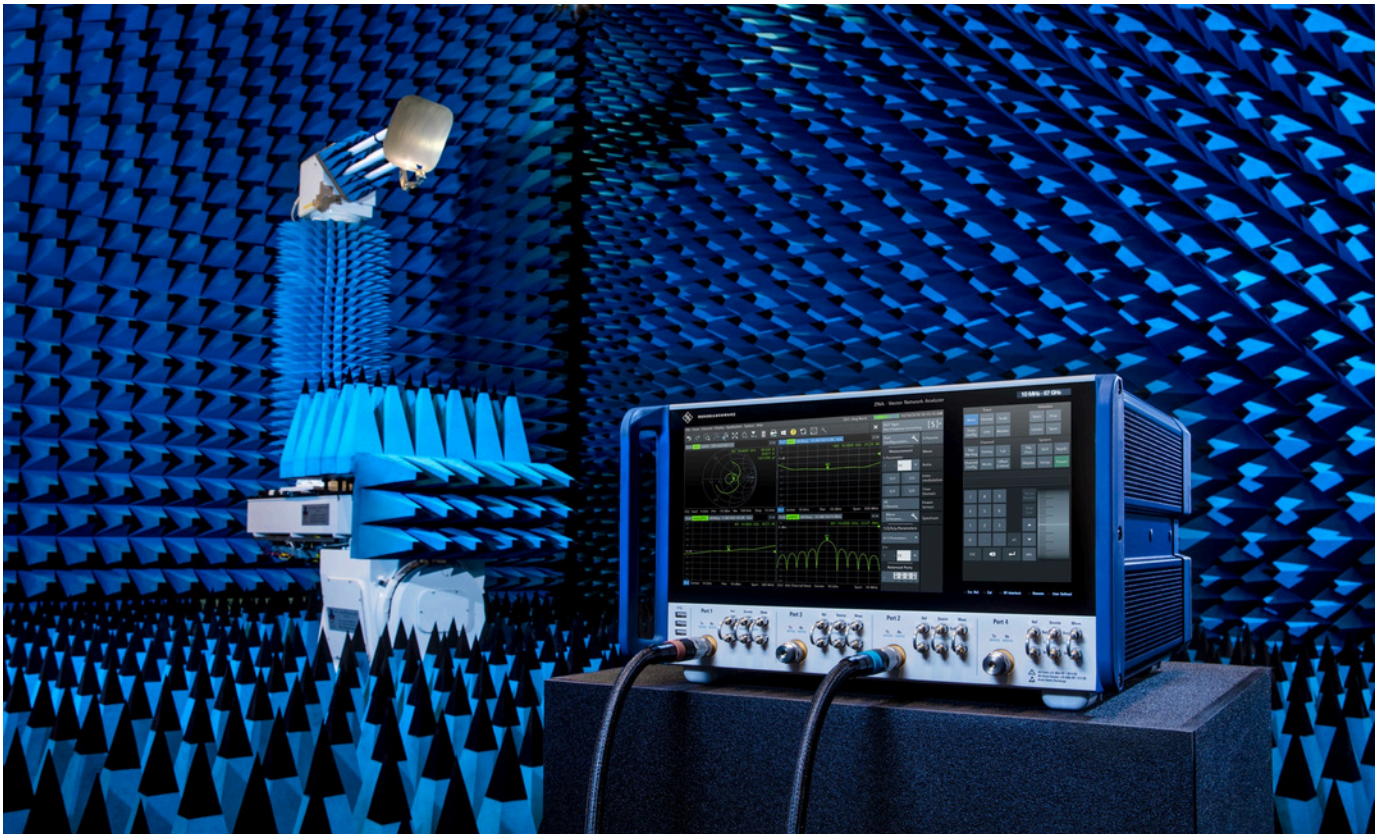
Partner system integration

With systems from Rohde & Schwarz and its partner companies, Rohde & Schwarz provides complete free-field, far-field and RCS test systems.



The sensitivity of the R&S®ZNA26/R&S®ZNA43 receivers can reach -150 dBm (lower frequency end, typical, at 1 Hz IFBW, direct channel access/reversed coupler, receiver step attenuator in 0 dB position). The sensitivity of the b1 and b2 receivers is increased further by using the R&S®ZNAxx-B302 and R&S®ZNAxx-B501 preamplifiers.

The R&S®ZNA forms the powerful core in antenna test systems



mmWave MEASUREMENTS

Frequency bands in the mmWave and terahertz ranges are used in many applications in the mobile communications, automotive, security, semiconductor and fundamental research sectors. Automotive radar at 77 GHz/79 GHz, mobile communications in the 5G frequency bands, and radars and sensors up to and beyond 100 GHz all require the characterization of active and passive components such as filters, amplifiers, mixers and antennas.

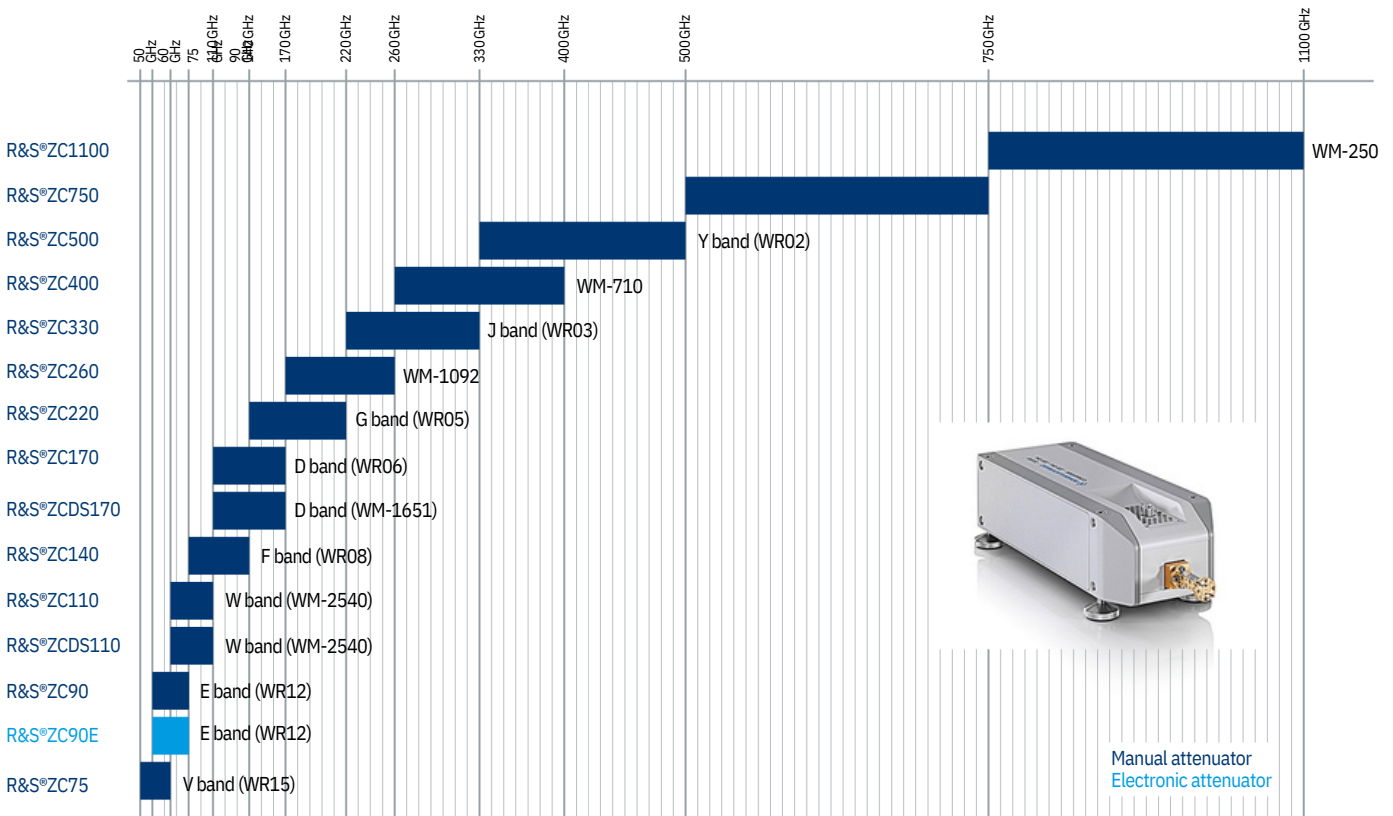
Frequency extension into the terahertz range

The R&S®ZVA-Zxxx and R&S®ZCxxx mmWave converters extend the R&S®ZNA frequency range up to 1.1 THz. Many applications, in particular on-wafer component characterization and antenna measurements, call for frequency converters with high output powers. The high operating frequencies of the components under test lead to significant losses in waveguides, probe tips and along the transmission path. The Rohde & Schwarz frequency converters feature high output powers and excellent dynamic range. They can be used to characterize active and passive DUTs.

Compact systems with dedicated options

The optional R&S®ZNA-B8 mmWave converter LO output makes the analyzer's internal LO signal available at the rear panel. The signal comes from the standard LO or, when a second internal LO is installed, from the 2nd LO. It provides up to +25 dBm output power, which is sufficient to feed up to four frequency converters connected to the R&S®ZNA. Configuration of the R&S®ZNA-B8 output for use with mmWave converters requires the R&S®ZNA-K8 option (mmWave converter support). The output power can be automatically calibrated to compensate for any losses introduced by cables and splitters. With the R&S®ZNA-B26 direct IF access option installed, the converters' measurement and reference signals are directly fed to the analyzer's IF path. The R&S®ZNAxx-B16 direct source and receiver access option can be used alternatively.

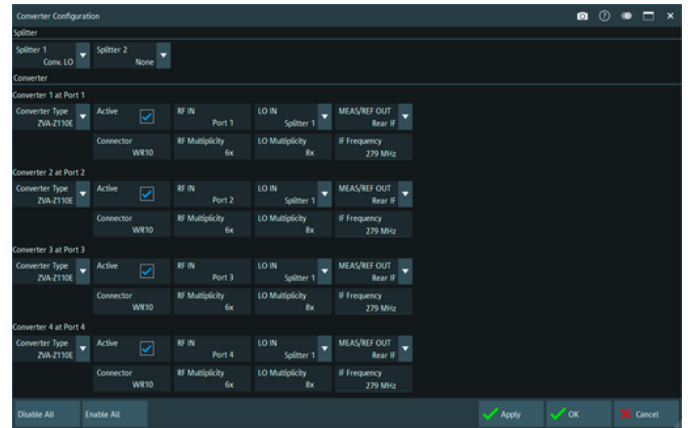
Overview of R&S®ZCxxx mmWave converters



Special features of R&S®ZVA-Zxxx and R&S®ZCxxx mmWave converters

- ▶ High output powers and wide dynamic range
- ▶ Easy configuration via straightforward dialog
- ▶ Multiport measurements with up to four converters without an external source
- ▶ Variable output power (manual adjustment with screw and/or control of output power by varying the input power)
- ▶ Amplifier characterization, power sweeps, compression point measurements
- ▶ R&S®ZNA-K1 spectrum analysis support in the mmWave range
- ▶ Phase coherence stimulation
- ▶ Absolute level calibration using power test heads from Rohde & Schwarz and Eriksson PM5/PM5B
- ▶ Automatic level control (ALC) usable in the mmWave range
- ▶ Pulsed measurements
- ▶ On-wafer component characterization, integration into MPI Corporation and FormFactor wafer prober systems
 - ▶ Waveguide calibration kits (with or without sliding match) for all frequency bands of the converters
- ▶ High time and temperature stability
- ▶ Frequency-converting measurements ¹⁾
- ▶ Integration in (active) load pull test systems from Focus Microwaves and Maury Microwave
- ▶ Supported by mmWave material test systems from company SwissTo12
- ▶ Intermodulation measurements with R&S®ZCDS110 and R&S®ZCDS170 dual source mmWave converters

¹⁾ Converters with different frequency ranges can be used; external source(s) may be required, depending on setup/configuration.

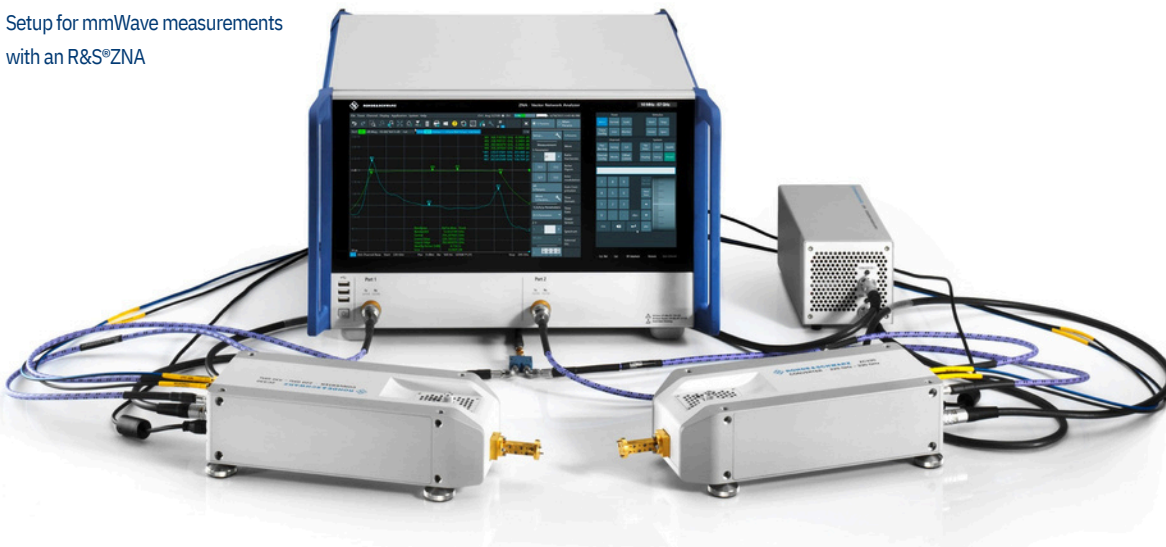


Software configuration

Software configuration

- ▶ Straightforward dialog for configuring 1-port to 4-port mmWave converter setups
- ▶ Menu-based selection of R&S®ZVA-Zxxx converter(s); automatic detection of R&S®ZCxxx converter(s)
- ▶ Configuration of customer's mmWave converters
- ▶ Support of Rohde & Schwarz and Erickson power sensors for absolute power level calibration up to 1.1 THz
- ▶ Configuration of frequency-converting measurements ¹⁾

Setup for mmWave measurements with an R&S®ZNA

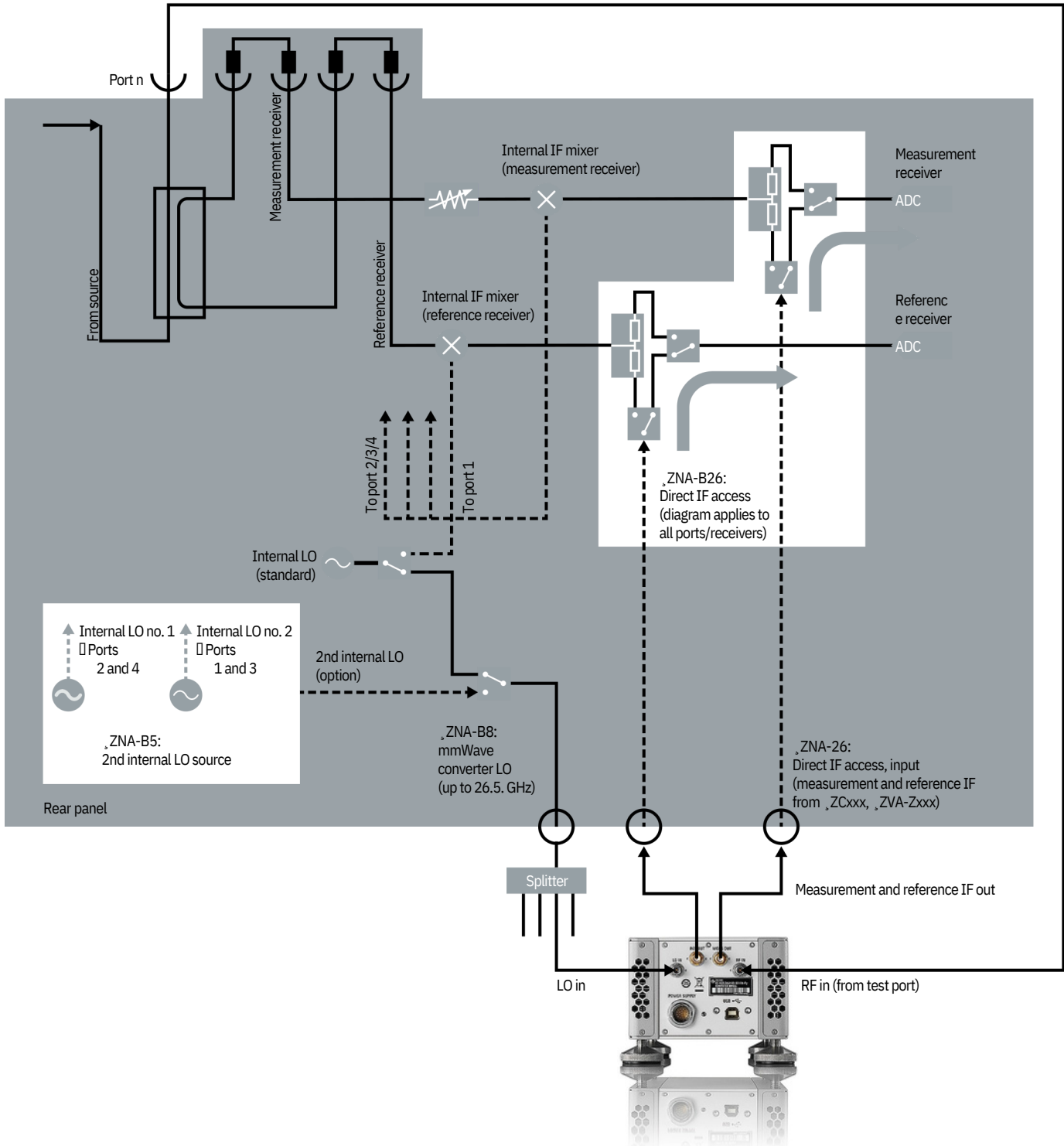


Hardware configuration

- ▶ Rear panel LO output up to +25 dBm (R&S®ZNA-B8 mmWave converter LO option) reliably provides converters with desired power even with long cables and LO splitters
- ▶ Use of direct IF inputs on R&S®ZNA rear panel

- ▶ Direct IF inputs with 1 GHz bandwidth for flexible integration of customer's mmWave converters
- ▶ Compact test setups: 2/4-port mmWave converter setups with 2/4-port R&S®ZNA, no external source or adapter box required

Hardware configuration for mmWave measurements



4-port R&S®ZNA67EXT single sweep system up to 110 GHz



**R&S®ZNA67EXT vector network analyzer system:
single sweep system up to 110 GHz**

Some applications, such as on-wafer transistor characterization, require a single sweep from 10 MHz to 110 GHz with only one probe contact. The R&S®ZNA67EXT system is an extension of the R&S®ZNA67 with converters and diplexers to allow a single sweep from 10 MHz to 110 GHz with a coaxial 1 mm connector.

The system is available with two or four 1 mm test ports. The 2-port system can be configured with a 2-port R&S®ZNA67 or a 4-port R&S®ZNA67 base unit, whereas the 4-port system always requires a 4-port R&S®ZNA67 base unit.

All systems are available in standard power configuration not subject to export control and high-power systems subject to export control.

TVAC TESTING AND SATELLITE TVAC TESTING

The R&S® ZNA provides reliable results with thermal vacuum chamber (TVAC) testing and satellite TVAC testing.

A VNA system error correction (SEC) requires the connection of single calibration standards or an automatic calibration unit, but for subsequent measurement, the calibration equipment is disconnected and the DUT is connected instead. However, there are mainly two application cases where this procedure is not applicable: TVAC testing/satellite TVAC testing and multipoint testing/production testing.

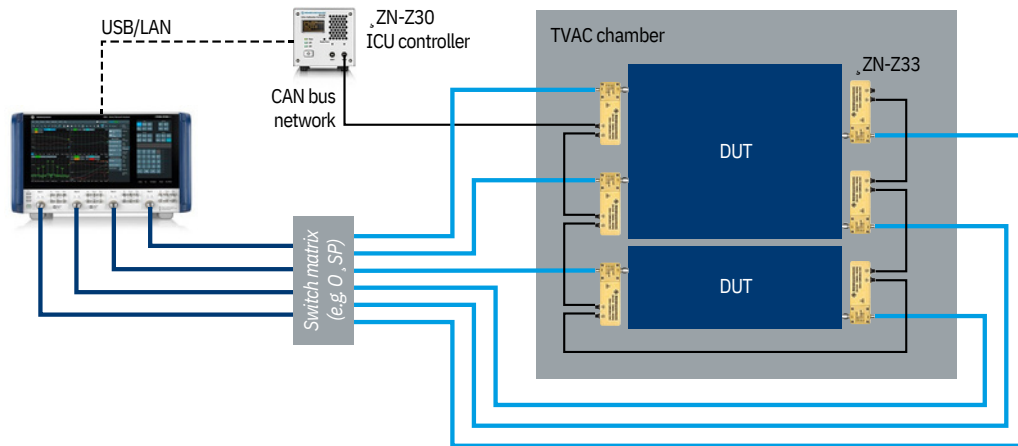
TVAC testing/satellite TVAC testing: After evacuation and at every change of temperature, the RF response of test set components inside the chamber is potentially changed. However, there is no access to the reference

planes in the TVAC chamber to connect calibration equipment for a recalibration.

Multipoint testing/production testing: Especially in cases where there is a combination of both multipoint DUT in production and numerous cables that are continuously moved, frequent recalibration is required. The R&S® ZN-Z3xx inline calibration units are designed to stay permanently in the reference plane, thus enabling frequent remote-controlled recalibration at a keystroke, without the need to access the test setup.

Schematic TVAC setup with Rohde & Schwarz inline calibration units

The inline calibration units (ICU) are connected to the DUT inside the chamber. Recalibration at each change of temperature and path switching is controlled by the R&S® ZNA and the R&S® ZN-Z30 ICU controller.



R&S® ZNA benefits for TVAC testing/satellite TVAC testing

Function/feature

Firmware integration

Benefits

- ▶ Base calibration and recalibration included in the R&S® SMARTerCal environment
- ▶ Calibration update in TVAC chambers and with multipoint setups in a few keystrokes

CAN bus network structure

- ▶ A single controller supports up to 48 modules (corresponds to 48 connections)
- ▶ Distances up to 20 m possible
- ▶ Plug & play configuration

Extended feature range: power calibration (base calibration only), deembedding, mixer measurements

- ▶ Get accurate stimulation power even in TVAC chamber testing
- ▶ Correct for auxiliary components (adapters, splitter)
- ▶ Converter testing in TVAC

MULTIPOINT EXTENSIONS

With predefined portgroups and USB autodetection, multipoint systems based on R&S®ZN-Z8x switch matrices are configured in a few key strokes. RF switch and control tasks are quick and easy to perform with the modular R&S®OSP open switch and control platform. The latest R&S®OSP generation comes with an extended range of modules, allowing an even wider variety of RF wiring configurations.

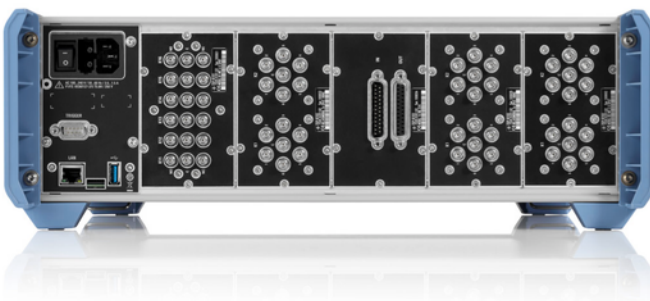
R&S®ZN-Z84 switch matrix, plug & play controlled (with 24 ports optional)



R&S®OSP220 and R&S®OSP230 open switch and control platforms



Rear view of the R&S®OSP320



A wide range of applications – from passive distributions to antenna beamforming arrays – requires multipoint extension modules. The R&S®ZNA supports plug & play solutions as well as individually configurable switch matrices:

- ▶ The R&S®ZN-Z8x switch matrices are configurable with 6 to 24 ports and full crossbar, ranging up to 8 GHz/20 GHz
- ▶ The R&S®OSP open switch and control platform offers a freely configurable framework. Switch modules ranging from basic single pole, double throw (SPDT) to multiple I/O design can be combined in one rack frame and configured by channel as required.

R&S®ZNA benefits using multipoint extensions

Function/feature

R&S®ZN-Z8x switch matrices with up to 8 GHz (6 to 24 ports) or 20 GHz (6 and 12 ports)

R&S®OSP open switch and control platform with up to 6 switch modules, combination of single pole, double throw (SPDT) and throughout multiple I/O design

Benefits

Easy plug & play configuration of predefined sets of port groups

- ▶ Application-specific combination of switch modules
- ▶ Active multipoint device testing up to 67 GHz

ORDERING INFORMATION

| Designation | Type | Frequency range | Order No. | Remarks |
|--|---------------|---------------------|--------------|---|
| Base units | | | | |
| Vector network analyzer, 2 ports, 26.5 GHz, 3.5 mm connectors | R&S®ZNA26 | 10 MHz to 26.5 GHz | 1332.4500.22 | |
| Vector network analyzer, 4 ports, 26.5 GHz, 3.5 mm connectors | R&S®ZNA26 | 10 MHz to 26.5 GHz | 1332.4500.24 | |
| Vector network analyzer, 2 ports, 43.5 GHz, 2.92 mm connectors | R&S®ZNA43 | 10 MHz to 43.5 GHz | 1332.4500.42 | |
| Vector network analyzer, 2 ports, 43.5 GHz, 2.4 mm connectors | R&S®ZNA43 | 10 MHz to 43.5 GHz | 1332.4500.43 | |
| Vector network analyzer, 4 ports, 43.5 GHz, 2.92 mm connectors | R&S®ZNA43 | 10 MHz to 43.5 GHz | 1332.4500.44 | |
| Vector network analyzer, 4 ports, 43.5 GHz, 2.4 mm connectors | R&S®ZNA43 | 10 MHz to 43.5 GHz | 1332.4500.45 | |
| Vector network analyzer, 2 ports, 50 GHz, 2.4 mm connectors | R&S®ZNA50 | 10 MHz to 50 GHz | 1332.4500.52 | |
| Vector network analyzer, 4 ports, 50 GHz, 2.4 mm connectors | R&S®ZNA50 | 10 MHz to 50 GHz | 1332.4500.54 | |
| Vector network analyzer, 2 ports, 67 GHz, 1.85 mm connectors | R&S®ZNA67 | 10 MHz to 67 GHz | 1332.4500.62 | |
| Vector network analyzer, 4 ports, 67 GHz, 1.85 mm connectors | R&S®ZNA67 | 10 MHz to 67 GHz | 1332.4500.64 | |
| Options | | | | |
| Direct source and receiver access, for R&S®ZNA26 (2 ports) | R&S®ZNA26-B16 | 100 kHz to 26.5 GHz | 1332.4581.22 | |
| Direct source and receiver access, for R&S®ZNA26 (4 ports) | R&S®ZNA26-B16 | 100 kHz to 26.5 GHz | 1332.4581.24 | |
| Direct source and receiver access, for R&S®ZNA43 (2 ports) | R&S®ZNA43-B16 | 100 kHz to 43.5 GHz | 1332.4581.42 | |
| Direct source and receiver access, for R&S®ZNA43 (4 ports) | R&S®ZNA43-B16 | 100 kHz to 43.5 GHz | 1332.4581.44 | |
| Direct source and receiver access, for R&S®ZNA50 (2 ports) | R&S®ZNA50-B16 | 10 MHz to 50 GHz | 1332.4581.52 | |
| Direct source and receiver access, for R&S®ZNA50 (4 ports) | R&S®ZNA50-B16 | 10 MHz to 50 GHz | 1332.4581.54 | |
| Direct source and receiver access, for R&S®ZNA67 (2 ports) | R&S®ZNA67-B16 | 10 MHz to 67 GHz | 1332.4581.62 | |
| Direct source and receiver access, for R&S®ZNA67 (4 ports) | R&S®ZNA67-B16 | 10 MHz to 67 GHz | 1332.4581.64 | |
| Source step attenuator, port n, for R&S®ZNA26 | R&S®ZNA26-B2n | 10 MHz to 26.5 GHz | 1332.4630.2n | n designates the port number |
| Source step attenuator, port n, for R&S®ZNA43 | R&S®ZNA43-B2n | 10 MHz to 43.5 GHz | 1332.4646.2n | (1/2/3/4) n designates the port number (1/2/3/4) n designates the |
| Source step attenuator, port n, for R&S®ZNA50 | R&S®ZNA50-B2n | 10 MHz to 50 GHz | 1332.5007.2n | port number (1/2/3/4) n designates |
| Source step attenuator, port n, for R&S®ZNA67 | R&S®ZNA67-B2n | 10 MHz to 67 GHz | 1332.5013.2n | the port number (1/2/3/4) n |
| Receiver step attenuator, port n, for R&S®ZNA26 | R&S®ZNA26-B3n | 10 MHz to 26.5 GHz | 1332.4700.3n | designates the port number (1/2/3/4) n |
| Receiver step attenuator, port n, for R&S®ZNA43 | R&S®ZNA43-B3n | 10 MHz to 43.5 GHz | 1332.4717.3n | n designates the port number |
| Receiver step attenuator, port n, for R&S®ZNA50 | R&S®ZNA50-B3n | 10 MHz to 50 GHz | 1332.5020.3n | (1/2/3/4) n designates the port |
| Receiver step attenuator, port n, for R&S®ZNA67 | R&S®ZNA67-B3n | 10 MHz to 67 GHz | 1332.5036.3n | number (1/2/3/4) n designates the |
| Internal pulse modulator, port n, for R&S®ZNA26 | R&S®ZNA26-B4n | 10 MHz to 26.5 GHz | 1332.4775.4n | port number (1/2/3/4) n designates |
| 6 | R&S®ZNA43-B4n | 10 MHz to 43.5 GHz | 1332.4781.4n | the port number (1/2/3/4) n |
| Internal pulse modulator, port n, for R&S®ZNA43 | R&S®ZNA50-B4n | 10 MHz to 50 GHz | 1332.5088.4n | designates the port number (1/2/3/4) |
| 3 | R&S®ZNA67-B4n | 10 MHz to 67 GHz | 1332.5094.4n | n designates the port number (1/2/3/4) |
| Internal pulse modulator, port n, for R&S®ZNA50 | R&S®ZNA26-B3 | 10 MHz to 26.5 GHz | 1332.4523.02 | n designates the port number (1/2/3/4) n designates the port number (1/2/3/4) |
| 0 | R&S®ZNA43-B3 | 10 MHz to 43.5 GHz | 1332.4617.02 | |
| 7 | R&S®ZNA50-B3 | 10 MHz to 50 GHz | 1332.4981.02 | |
| 3rd and 4th internal source, for R&S®ZNA26 (4 ports) | R&S®ZNA67-B3 | 10 MHz to 67 GHz | 1332.4998.02 | |
| 3rd and 4th internal source, for R&S®ZNA43 (4 ports) | | | | |
| 3rd and 4th internal source, for R&S®ZNA50 (4 ports) | | | | |
| 3rd and 4th internal source, for R&S®ZNA67 (4 ports) | | | | |

| Designation | Type | Frequency range | Order No. | Remarks |
|--|----------------|--------------------|----------------------------------|---|
| 2nd LO and RF source, for R&S®ZNA26 (2 ports) | R&S®ZNA26-B52 | 10 MHz to 26.5 GHz | 1332.6503.0 | |
| 2nd LO and RF source, for R&S®ZNA40 (2 ports) | R&S®ZNA40-B52 | 10 MHz to 43.5 GHz | 2 | |
| 2nd LO and RF source, for R&S®ZNA50 (2 ports) | R&S®ZNA50-B52 | 10 MHz to 50 GHz | 1332.6510.0 | |
| 2nd LO and RF source, for R&S®ZNA67 (2 ports) | R&S®ZNA67-B52 | 10 MHz to 67 GHz | 2 | |
| Direct source monitor access, port 1, for R&S®ZNA26 | R&S®ZNA26-B161 | 10 MHz to 26.5 GHz | 1332.6526.0 | 2-port and 4-port R&S®ZNA, requires R&S®ZNA 26 - B16, R&S®ZNA 26 - B21 |
| Direct source monitor access, port 1 and port 3, for R&S®ZNA26 | R&S®ZNA26-B163 | 10 MHz to 26.5 GHz | 2 1332.4832.63 | 4 - port R&S®ZNA, requires R&S®ZNA 26 - B16, R&S®ZNA 26 - B21, R&S®ZNA 26 - B23 |
| Direct source monitor access, port 1, for R&S®ZNA43 | R&S®ZNA43-B161 | 10 MHz to 43.5 GHz | 2 1332.4303.51 1332.4823.5 | 2-port and 4-port R&S®ZNA, requires R&S®ZNA43-B16, R&S®ZNA43-B21 |
| Direct source monitor access, port 1 and port 3, for R&S®ZNA43 ²⁾ | R&S®ZNA43-B163 | 10 MHz to 43.5 GHz | 1 1332.4830.53 | 4 - port R&S®ZNA, requires R&S®ZNA43-B16, R&S®ZNA43-B21, R&S®ZNA43-B23 |
| Direct source monitor access, port 1, for R&S®ZNA50 | R&S®ZNA50-B161 | 10 MHz to 50 GHz | 1332.5107.51 | 2-port and 4-port R&S®ZNA, requires R&S®ZNA50 -B16, R&S®ZNA50 -B21 |
| Direct source monitor access, port 1 and port 3, for R&S®ZNA50 | R&S®ZNA50-B163 | 10 MHz to 50 GHz | 1332.5107.53 | 4 - port R&S®ZNA, requires R&S®ZNA50-B16, R&S®ZNA50-B21, R&S®ZNA50 -B23 |
| Direct source monitor access, port 1, for R&S®ZNA67 | R&S®ZNA67-B161 | 10 MHz to 67 GHz | 1332.5113.51 | 2-port and 4 -por t R&S®ZNA, requires R&S®ZNA67-B16, R&S®ZNA67-B21 |
| Direct source monitor access, port 1 and port 3, for R&S®ZNA67 | R&S®ZNA67-B163 | 10 MHz to 67 GHz | 1332.5113.53 | 4 -por t R&S®ZNA, requires R&S®ZNA67-B16, R&S®ZNA67-B21, R&S®ZNA67-B23 |
| Low-noise preamplifier at receiver, port 2, for R&S®ZNA26 | R&S®ZNA26-B302 | 10 MHz to 26.5 GHz | 1332.4752.12 | re quires R&S®ZNA 26 - B 32 and R&S®ZNA 26 - B16 |
| Low-noise preamplifier at receiver, port 2, for R&S®ZNA43 | R&S®ZNA43-B302 | 10 MHz to 43 GHz | 1332.4769.12 | re quire s R&S®ZNA 4 3 - B 32 and R&S®ZNA43-B16 |
| Low noise preamplifier at receiver, port 2, for R&S®ZNA50 | R&S®ZNA50-B302 | 10 MHz to 50 GHz | 1332.4798.12 | requires R&S®ZNA50 -B32 and R&S®ZNA50-B16; export restricted, combinable with R&S®ZNA-K1 |
| Low noise preamplifier at receiver, port 2, for R&S®ZNA50 | R&S®ZNA50-B312 | 10 MHz to 50 GHz | 1332.5659.02 | requires R&S®ZNA50 -B32 and R&S®ZNA50-B16; not export restricted, not combinable with R&S®ZNA-K1 |
| Low noise preamplifier at receiver, port 2, for R&S®ZNA67 | R&S®ZNA67-B302 | 10 MHz to 67 GHz | 1332.4817.12 | requires R&S®ZNA67-B32 and R&S®ZNA67-B16; export restricted, combinable with R&S®ZNA-K1 |
| Low noise preamplifier at receiver, port 2, for R&S®ZNA67 | R&S®ZNA67-B312 | 10 MHz to 67 GHz | 1332.5665.02 | requires R&S®ZNA67-B32 and R&S®ZNA67-B16; not export restricted, not combinable with R&S®ZNA-K1 |
| Low-power spurious reduction, port 1, for R&S®ZNA26 | R&S®ZNA26-B501 | 10 MHz to 26.5 GHz | 1332.5220.11 | re quire s R&S®ZNA 26 - B 31 |
| Low-power spurious reduction, port 1, for R&S®ZNA43 | R&S®ZNA43-B501 | 10 MHz to 43.5 GHz | 1332.5236.11 | requires R&S®ZNA43-B31 |
| Low power spurious reduction, port 1, for R&S®ZNA50 | R&S®ZNA50-B501 | 10 MHz to 50 GHz | 1332.5242.11 | re quire s R&S®ZNA 50 - B 31 |
| Low power spurious reduction, port 1, for R&S®ZNA50 | R&S®ZNA50-B511 | 10 MHz to 50 GHz | 1332.5671.02 | re quire s R&S®ZNA 50 - B 31 |
| Low power spurious reduction, port 1, for R&S®ZNA67 | R&S®ZNA67-B501 | 10 MHz to 67 GHz | 1332.5259.11 | requires R&S®ZNA67-B31 |
| Low power spurious reduction, port 1, for R&S®ZNA67 | R&S®ZNA67-B511 | 10 MHz to 67 GHz | 1332.5688.02 | requires R&S®ZNA67-B31 |
| Low power spurious reduction, port 1, for R&S®ZNA67 | R&S®ZNA26-B212 | 10 MHz to 26.5 GHz | 1332.5265.02 | 2-port R&S®ZNA only; requires R&S®ZNA 26 - B52 and R&S®ZNA 26 - B21 |
| Internal combiner, port 1 and port 2, for R&S®ZNA26 (2 ports) | R&S®ZNA43-B212 | 10 MHz to 43.5 GHz | 1332.5271.02 | 2-port R&S®ZNA only; requires R&S®ZNA 4 3 - B52 and R&S®ZNA 4 3 - B21 |
| Internal combiner, port 1 and port 2, for R&S®ZNA43 (2 ports) | R&S®ZNA50-B212 | 10 MHz to 50 GHz | 1332.5288.02 | 2-port R&S®ZNA only; requires R&S®ZNA50 -B52 and R&S®ZNA50 -B21 |
| Internal combiner, port 1 and port 2, for R&S®ZNA50 (2 ports) | R&S®ZNA67-B212 | 10 MHz to 67 GHz | 1332.5294.02 | 2-port R&S®ZNA only; requires R&S®ZNA67-B52 and R&S®ZNA67-B21 |
| Internal combiner, port 1 and port 2, for R&S®ZNA67 (2 ports) | R&S®ZNA26-B213 | 10 MHz to 26.5 GHz | 1332.4846.13 | 4 - por t R&S®ZNA only; re quires R&S®ZNA 26 - B21 and R&S®ZNA 26 - B23 |
| Internal combiner, port 1 and port 3, for R&S®ZNA26 (4 ports) | R&S®ZNA43-B213 | 10 MHz to 43.5 GHz | 1332.4869.13 | 4 - por t R&S®ZNA only; re quires R&S®ZNA 4 3 - B21 and R&S®ZNA 4 3 - B23 |
| Internal combiner, port 1 and port 3, for R&S®ZNA43 (4 ports) | R&S®ZNA50-B213 | 10 MHz to 50 GHz | 1332.5042.13 | 4 - por t R&S®ZNA only; re quires R&S®ZNA50 -B21 and R&S®ZNA50 -B23 |
| Internal combiner, port 1 and port 3, for R&S®ZNA50 (4 ports) | R&S®ZNA67-B213 | 10 MHz to 67 GHz | 1332.5065.13 | 4 - por t R&S®ZNA only; re quires R&S®ZNA67-B21 and R&S®ZNA67-B23 |
| Internal combiner, port 1 and port 3, for R&S®ZNA67 (4 ports) | R&S®ZNA-B4 | | 1332.4530.02 | |
| Internal combiner, port 1 and port 3, for R&S®ZNA67 (4 ports) | R&S®ZNA-B5 | | 1332.4675.02 | |
| Precision frequency reference (OCXO) Data streaming memory 2nd internal LO source for R&S®ZNA (4 ports) | R&S®ZNA-B7 | | 1332.4546.02 | increases the number of receivers that can be used in parallel for pulse profile measurements (depending on IF bandwidth) |

| Designation | Type | Frequency range | Order No. | Remarks |
|---|-------------------|--------------------|--------------|---|
| mmWave converter LO | R&S®ZNA-B8 | 10 MHz to 26.5 GHz | 1332.4652.02 | flexible configuration for all mmWave converters, mixers, etc. |
| mmWave extender LO output | R&S®ZNA67-B80 | 10 MHz to 26.5 GHz | 1332.5836.02 | supports mmWave converters only from 110 GHz to 117 GHz to meet export restrictions to dedicated regions |
| Metrology configuration, for R&S®ZNA26 (2 ports) | R&S®ZNA26-B10 | | 1332.4698.22 | |
| Metrology configuration, for R&S®ZNA26 (4 ports) | R&S®ZNA26-B10 | | 1332.4698.24 | |
| Metrology configuration, for R&S®ZNA43 (2 ports) | R&S®ZNA43-B10 | | 1332.4698.42 | 2.92 mm connectors |
| Metrology configuration, for R&S®ZNA43 (2 ports) | R&S®ZNA43-B10 | | 1332.4698.43 | 2.4 mm connectors |
| Metrology configuration, for R&S®ZNA43 (4 ports) | R&S®ZNA43-B10 | | 1332.4698.44 | 2.92 mm connectors |
| Metrology configuration, for R&S®ZNA43 (4 ports) | R&S®ZNA43-B10 | | 1332.4698.45 | 2.4 mm connectors |
| Metrology configuration, for R&S®ZNA50 (2 ports) | R&S®ZNA50-B10 | | 1332.4698.52 | |
| Metrology configuration, for R&S®ZNA50 (4 ports) | R&S®ZNA67-B10 | | 1332.4698.54 | |
| Metrology configuration, for R&S®ZNA67 (2 ports) | R&S®ZNA67-B10 | | 1332.4698.62 | |
| Metrology configuration, for R&S®ZNA67 (4 ports) | R&S®ZNA67-B10 | | 1332.4698.64 | |
| Device control | R&S®ZNA-B12 | | 1332.4552.02 | |
| RFFE GPIO interface | R&S®ZNA-B15 | | 1332.4575.02 | |
| RFFE GPIO interface, including voltage/current measurement | R&S®ZNA-B15 | | 1332.4575.03 | |
| Direct IF access | R&S®ZNA-B26 | | 1332.4598.02 | |
| Trigger and control I/O board | R&S®ZNA-B91 | | 1332.4800.02 | |
| Spectrum analyzer mode | R&S®ZNA-K1 | | 1332.5320.02 | |
| Time domain analysis (TDR) | R&S®ZNA-K2 | | 1332.5336.02 | |
| Extended time domain analysis (including eye diagram) | R&S®ZNA-K20 | | 1332.4746.02 | requires R&S®ZNA-K2 |
| Continuous data recording | R&S®ZNA-K28 | | 1332.5613.02 | |
| Scalar mixer and arbitrary frequency-converting measurements | R&S®ZNA-K4 | | 1332.5342.02 | |
| Vector corrected converter measurements (without reference mixer and phase reference) | R&S®ZNA-K5 | | 1332.5359.02 | requires R&S®ZNA-K4 |
| Phase coherent source control | R&S®ZNA-K6 | | 1332.5413.02 | |
| True differential mode Speed improvement | R&S®ZNA-K61 | | 1332.5442.02 | requires R&S®ZNA-K6 |
| Measurements on pulsed signals Increased IF bandwidth 30 MHz mmWave converter support | R&S®ZNA-K66 | | 1332.5820.02 | |
| | R&S®ZNA-K7 | | 1332.5371.02 | requires R&S®ZNA-K17 |
| | R&S®ZNA-K17 | | 1332.5459.02 | |
| | R&S®ZNA-K8 | | 1332.5388.02 | |
| Group delay measurements on frequency converters without LO access | R&S®ZNA-K9 | | 1332.5394.02 | requires R&S®ZNA-K4 and options to generate a two-tone signal; ▶ 2-port R&S®ZNA: R&S®ZNAxx-B52, R&S®ZNA x x- B21, R&S®ZNA x x- B212 ▶ 4-port R&S®ZNA: R&S®ZNAxx-B16 and R&S®ZNAxx-Z9 cable set or R&S®ZNA x x- B213 internal combiner, R&S®ZNAxx-B21/-B23 |
| 1 MHz frequency resolution Noise figure measurements | R&S®ZNA-K19 | | 1332.5513.0 | |
| Uncertainty analysis | R&S®ZNA-K30 | | 2 | |
| analysis, preinstalled Security write protection | R&S®ZNA-K50 | | 1332.5465.0 | METAS tool user provided |
| SNP assistant EaZy deembedding (EZD) In-situ deembedding (ISD) | R&S®ZNA-K50P | | 2 | METAS tool preinstalled |
| Smart fixture deembedding (SFD) Delta- | R&S®ZNA-K51 | | 2 | |
| L PCB characterization Health and utilization monitoring service (HUMS) | R&S®ZNA-K100 | | 1332.5594.0 | 2 |
| Windows 11 24H2 upgrade kit | R&S®ZNA-K210 | | 1332.5559.0 | 2 |
| mmWave converters | K210 | | 2 | |
| Converter WR15, one module | R&S®ZNA-K220 | | 1338.9327.0 | |
| Converter WR12, one module | K220 | | 2 | upgrade to IPS15, including SSD |
| Converter WR12, one module Converter WM-2540, one module Converter WM-2540 | R&S®ZNA-R&S®ZNA70 | 50 GHz to 75 GHz | 1339.3897.0 | converters require R&S®ZNA-K8 |
| | R&S®ZNA70 | 50 GHz to 75 GHz | 2323.8259.0 | |
| | R&S®ZNA90 | 60 GHz to 90 GHz | 2339.3900.0 | |
| Converter WM-2032, one module | R&S®ZNA90E | 60 GHz to 90 GHz | 2323.7600.0 | |
| | R&S®ZNA110 | 75 GHz to 110 GHz | 2339.3916.0 | |
| | R&S®ZNA110 | 75 GHz to 110 GHz | 2323.7600.0 | combiner for 2-tone signal included |
| | R&S®ZNA140 | 90 GHz to 140 GHz | 2339.3922.0 | |
| | | | 2323.7617.0 | |
| | | | 2332.5607.0 | |
| | | | 2354.5322.0 | |
| | | | 2357.4204.0 | |

| Designation | Type | Frequency range | Order No. | Remarks |
|--|-------------|---------------------|--------------|--|
| Converter WM-1651, one module | R&S®ZC170 | 110 GHz to 170 GHz | 1323.7630.0 | |
| Converter WM-1651, one module | R&S®ZC170 | 110 GHz to 170 GHz | 2 | only for R&S®ZNA43, R&S®ZNA50, R&S®ZNA67 |
| Converter WM-1651 | R&S®ZCDS170 | 110 GHz to 170 GHz | 1323.7630.0 | combiner for 2-tone signal included |
| Converter WM-1295, one module | R&S®ZC220 | 140 GHz to 220 GHz | 3 | |
| Converter WM-1092, one module | R&S®ZC260 | 170 GHz to 260 GHz | 1354.5522.0 | |
| Converter WM-864, one module | R&S®ZC330 | 220 GHz to 330 GHz | 2 | |
| Converter WM-710, one module | R&S®ZC400 | 260 GHz to 400 GHz | 1323.7646.0 | |
| Converter WM-570, one module | R&S®ZC500 | 330 GHz to 500 GHz | 2 | |
| Converter WM-570, one module | R&S®ZC500 | 330 GHz to 500 GHz | 3628.5682.0 | only for R&S®ZNA43, R&S®ZNA50, R&S®ZNA67 |
| Converter WM-750, one module | R&S®ZC750 | 500 GHz to 750 GHz | 2 | |
| Converter WM-250, one module | R&S®ZC1100 | 750 GHz to 1100 GHz | 1323.7669.0 | |
| mmWave receivers | | | 2 | receivers require R&S®ZNA-K8 |
| Receiver WR12, one module | R&S®ZRX90 | 60 GHz to 90 GHz | 3656.9220.0 | |
| Receiver WM-2540 (WR10), one module | R&S®ZRX110 | 75 GHz to 110 GHz | 3658.5368.0 | |
| Receiver WM-2032 (WR08), one module | R&S®ZRX140 | 90 GHz to 140 GHz | 2 | |
| Receiver WM-1651 (WR6.5), one module | R&S®ZRX170 | 110 GHz to 170 GHz | 1323.7681.0 | |
| Receiver WM-1295 (WR5.1), one module | R&S®ZRX220 | 140 GHz to 220 GHz | 3637.1511.0 | |
| Receiver WM-1092 (WR4.3), one module | R&S®ZRX260 | 170 GHz to 260 GHz | 2 | |
| Receiver WM-864 (WR3.4), one module | R&S®ZRX330 | 220 GHz to 330 GHz | 1323.7681.0 | |
| Receiver WM-710 (WR2.8), one module | R&S®ZRX400 | 260 GHz to 400 GHz | 3637.1528.0 | |
| Receiver WM-570, one module | R&S®ZRX500 | 330 GHz to 500 GHz | 2 | |
| Receiver WM-380 (WR1.5), one module | R&S®ZRX750 | 500 GHz to 750 GHz | 1323.7743.0 | |
| Receiver WM-250 (WR1.0), one module | R&S®ZRX110 | 750 GHz to 1100 GHz | 3622.0750.0 | |
| mmWave mini receivers | | | 2 | receivers require R&S®ZNA-K8 |
| Mini receiver WM-2540 (WR10), one module | R&S®ZRX110 | 75 GHz to 110 GHz | 3622.0748.0 | |
| Mini receiver WM-1651 (WR6.5), one module | L | 110 GHz to 170 GHz | 2 | |
| Mini receiver WM-1295 (WR5.1), one module | R&S®ZRX170 | 140 GHz to 220 GHz | 3688.8317.0 | |
| Mini receiver WM-864 (WR3.4), one module | L | 220 GHz to 330 GHz | 2 | |
| Mini receiver WM-570, one module | R&S®ZRX220 | 330 GHz to 500 GHz | 3622.0702.0 | |
| Mini receiver WM-380 (WR1.5), one module | L | 500 GHz to 750 GHz | 2 | |
| Calibration and verification | | | 3658.5928.0 | |
| Calibration kits (manual calibration) | L | | 2 | |
| Calibration kit, 3.5 mm, 50 Ω | R&S®ZRX500 | 0 Hz to 26.5 GHz | 3888.8808.0 | |
| Calibration kit, 2.92 mm, 50 Ω | Z235 | 0 Hz to 43.5 GHz | 2 | |
| Calibration kit, 2.4 mm, 50 Ω | R&S®ZRX750 | 0 Hz to 50 GHz | 3886.9068.0 | |
| Calibration kit, 1.85 mm, 50 Ω | Z229 | 0 Hz to 67 GHz | 2 | |
| Calibration kit, 1.0 mm, 50 Ω | R&S®ZN- | 0 Hz to 110 GHz | 1339.5002.0 | |
| Waveguide calibration kits | | | 2 | |
| Waveguide calibration kit WR15 (without sliding match) | R&S®ZV-WR15 | 50 GHz to 75 GHz | 1337.3500.0 | |
| Waveguide calibration kit WR15 (with sliding match) | Z218 | | 2 | |
| Waveguide calibration kit WR15 (with sliding match) | R&S®ZM-WR15 | 50 GHz to 75 GHz | 1307.3400.01 | |
| Waveguide calibration kit WR12 (without sliding match) | Z210 | | 2 | |
| Waveguide calibration kit WR12 (without sliding match) | R&S®ZV-WR12 | 60 GHz to 90 GHz | 1307.7700.10 | |
| Waveguide calibration kit WR12 (with sliding match) | R&S®ZV-WR12 | 60 GHz to 90 GHz | 1307.7700.11 | |
| Waveguide calibration kit WR10 (without sliding match) | R&S®ZV-WR10 | 75 GHz to 110 GHz | 1307.7100.10 | |
| Waveguide calibration kit WR10 (with sliding match) | R&S®ZV-WR10 | 75 GHz to 110 GHz | 1307.7100.11 | |
| Waveguide calibration kit WR08 (without sliding match) | R&S®ZV-WR08 | 90 GHz to 140 GHz | 1307.7900.10 | |
| Waveguide calibration kit WR08 (with sliding match) | R&S®ZV-WR08 | 90 GHz to 140 GHz | 1307.7900.11 | |
| Waveguide calibration kit WR06 (without sliding match) | R&S®ZV-WR06 | 110 GHz to 170 GHz | 1311.8807.10 | |
| Waveguide calibration kit WR06 (with sliding match) | R&S®ZV-WR06 | 110 GHz to 170 GHz | 1311.8807.11 | |

| Designation | Type | Frequency range | Order No. | Remarks |
|---|----------------------|---------------------|-----------------------------|--|
| Waveguide calibration kit WR05 (without sliding match) | R&S®ZV-WR05 | 140 GHz to 220 GHz | 1307.8106.10 | |
| Waveguide calibration kit WR05 (with sliding match) | R&S®ZV-WR05 | 140 GHz to 220 GHz | 1307.8106.11 | |
| Waveguide calibration kit WR03 (without sliding match) | R&S®ZV-WR03 | 220 GHz to 325 GHz | 1307.7300.30 | |
| Waveguide calibration kit WR03 (with sliding match) | R&S®ZV-WR03 | 220 GHz to 325 GHz | 1307.7300.31 | |
| Waveguide calibration kit WR02 (without sliding match) | R&S®ZV-WR02 | 325 GHz to 500 GHz | 1314.5550.10 | |
| Waveguide calibration kit WM-1092 | R&S®ZCWM-1092 | 170 GHz to 260 GHz | 3628.5699.02 | |
| Waveguide calibration kit WM-710 | R&S®ZCWM-710 | 260 GHz to 400 GHz | 1339.4070.02 | |
| Waveguide calibration kit WM-570 | R&S®ZCWM-570 | 330 GHz to 500 GHz | 1322.3099.10 | |
| Waveguide calibration kit WM-380 | R&S®ZCWM-380 | 500 GHz to 750 GHz | 1322.3101.02 | |
| Waveguide calibration kit WM-250 | R&S®ZCWM-250 | 750 GHz to 1100 GHz | 1322.3118.02 | |
| Calibration units (automatic calibration) | | | | |
| Calibration unit, 2 ports, 3.5 mm (f) | R&S®ZN-Z50 | 9 kHz to 26.5 GHz | 1335.6904.3 | |
| Calibration unit, 4 ports, 3.5 mm (f) | R&S®ZN-Z52 | 100 kHz to 26.5 GHz | 2 | |
| Calibration unit, 2 ports, 3.5 mm (f) | R&S®ZN-Z53 | 100 kHz to 26.5 GHz | 1335.6991.3 | |
| Calibration unit, 2 ports, 2.92 mm (f) | R&S®ZN-Z54 | 9 kHz to 40 GHz | 0 | characterized to 4.3.5 GHz |
| Calibration unit, 2 ports, 2.4 mm (f) | R&S®ZN-Z55 | 9 kHz to 50 GHz | 1335.7046.3 | |
| Calibration unit, 2 ports, 1.85 mm (f) | R&S®ZN- | 10 MHz to 67 GHz | 2 | |
| Inline calibration units (automatic calibration) | | | Z156 | 1335.7117.9 |
| Inline calibration unit controller | R&S®ZN- | | 2328.7609.0 | |
| Inline calibration unit, 40 GHz | Z30 | | 2335.7181.4 | |
| Inline calibration unit, 40 GHz, TVAC | R&S®ZN- | | 2328.7644.0 | |
| Comb generators (phase calibration reference) | | | Z33 | 2332.7239.0 |
| Comb generator, 2.92 mm (f) Comb generator, 1.85 mm (f) | R&S®ZN- | 10 MHz to 44 GHz | 1332.3000.0 | requires R&S®ZNA-B12 option |
| Verification kits | Z6644 | 10 MHz to 67 GHz | 2 | requires R&S®ZNA-B12 option |
| T-check verification device, 3.5 mm (f) | R&S®ZN- | | 1352.3000.6 | |
| T-check verification device, 2.92 mm (f) | R&S®ZN- | 45 MHz to 26.5 GHz | 2319.1018.0 | |
| T-check verification device, 2.4 mm (f to m) Verification kit, 3.5 mm | Z335 | 45 MHz to 40 GHz | 2 | |
| Verification kit, 2.92 mm Verification kit, 2.4 mm | R&S®ZV- | 45 MHz to 50 GHz | 1319.1024.0 | |
| Test cables | | | Z329 | 45 MHz to 26.5 GHz |
| 3.5 mm (f) to 3.5 mm (m), length: 0.6 m | R&S®ZV- | 45 MHz to 40 GHz | 1319.1030.0 | |
| 2.92 mm (f) to 2.92 mm (m), length: 0.6 m/1 m | R&S®ZV- | 45 MHz to 50 GHz | 2 | |
| 2.4 mm (f) to 2.4 mm (m), length: 0.6 m | R&S®ZV- | | 1319.1060.0 | |
| 3.5 mm (f) to 3.5 mm (m), length: 0.6 m/0.9 m/1.5 m | R&S®ZV- | 0 Hz to 26.5 GHz | 2301.7595.25 | |
| | R&S®ZV- | 0 Hz to 40 GHz | 1309.1608.05/38 | |
| | R&S®ZV- | 0 Hz to 50 GHz | 2301.7637.25 | |
| | R&S®ZV- | 0 Hz to 26.5 GHz | 1300.1020.04/36/ | |
| 2.92 mm (f) to 2.92 mm (m), length: 0.6 m/0.9 m | R&S®ZV-Z195 | 0 Hz to 40 GHz | 20 | |
| 2.92 mm (m) to 2.92 mm (m), length: 0.9 m | R&S®ZV-Z195 | 0 Hz to 40 GHz | 1306.4536.24/36 | recommended when using R&S®ZNA-B8 option |
| 1.85 mm (f) to 1.85 mm (m), length: 0.6 m/0.9 m | R&S®ZV-Z196 | 0 Hz to 67 GHz | 1306.4536.37 | |
| 1.85 mm (m) to 1.85 mm (m), length: 0.6 m/0.9 m | R&S®ZV-Z196 | 0 Hz to 67 GHz | 1306.4559.24/36 | |
| Hardware add-ons | | | | 1306.4559.25/37 |
| Calibration mixer, 2.92 mm (f) | R&S®ZN- | 10 MHz to 40 GHz | 1339.3800.0 | |
| Calibration mixer, 2.92 mm (f), delivery without wooden storage box | ZM292 | 10 MHz to 40 GHz | 2 | |
| mmWave adaption kit, for R&S®ZNA26/43, two converters | R&S®ZN- R&S®ZCAKN | | 1339.3800.0 1332.6178.43 | |
| mmWave adaption kit, for R&S®ZNA26/43, four converters | ZM292 R&S®ZCAKN | | 3 1332.6178.44 | |
| mmWave adaption kit, for R&S®ZNA50/67, two converters | R&S®ZCAKN | | 1332.6178.67 | |
| mmWave adaption kit, for R&S®ZNA50/67, four converters | R&S®ZCAKN | | 1332.6178.68 | |
| Torque wrench for 3.5/2.92/2.4/1.85 mm connector, 8 mm width, 0.9 Nm torque | R&S®ZN-ZTW | | 1328.8534.35 | |

| Designation | Type | Frequency range | Order No. | Remarks |
|--|----------------|-------------------|-----------------------------|---|
| Torque wrench, for R&S®ZNA test port connector, 19 mm width, 0.9 Nm torque | R&S®ZN-ZTW | | 1328.8534.19 | |
| Additional removable hard disk | R&S®ZNA-B19 | | 1332.4600.04 | with Windows 11 operating system |
| 19" rack adapter, pigeon blue | R&S®ZZA-KN6 | | 1175.3056.00 | |
| 19" rack adapter, violet blue | R&S®ZZA-KN6B | | 1703.1369.00 | color for instruments in the new housing design |
| Cable sets (to combine the signals from port 1 and port 3 of an R&S®ZNA (4 ports) to produce a two-tone signal, required for intermodulation measurements and embedded LO group delay measurements with R&S®ZNA-K9 option; required, if no internal combiner is installed) | | | | |
| Cable set for R&S®ZNA-K9 (3.5 mm for R&S®ZNA26) | R&S®ZNA26-Z9 | | 1332.4730.26 | |
| Cable set for R&S®ZNA-K9 (2.92 mm for R&S®ZNA43) | R&S®ZNA43-Z9 | | 1332.4730.43 | |
| Cable set for R&S®ZNA-K9 (2.4 mm for R&S®ZNA43) | R&S®ZNA43-Z9 | | 1332.4730.44 | |
| Cable set for R&S®ZNA-K9 (1.85 mm for R&S®ZNA50) | R&S®ZNA50-Z9 | | 1332.4730.50 | |
| Cable set for R&S®ZNA-K9 (1.85 mm for R&S®ZNA67) | R&S®ZNA67-Z9 | | 1332.4730.67 | |
| Tools | | | | |
| License dongle, PC software | R&S®ZNPC | | 1325.6601.0 | |
| R&S®ZNA simulation | R&S®ZNXSIM-K2 | | 2 | |
| Time domain analysis (TDR) for simulation | R&S®ZNXSIM-K22 | | 1338.1626.0 | |
| Vector network analyzer systems | | | 2 | |
| Vector network analyzer system, 110 GHz, 2 test ports, complete system based on R&S®ZNA67, 2-port model, standard power | R&S®ZNA67EXT | 10 MHz to 110 GHz | 1338.1632.0 1352.1888.12 | |
| Vector network analyzer system, 110 GHz, 2 test ports, complete system based on R&S®ZNA67, 4-port model, standard power | R&S®ZNA67EXT | 10 MHz to 110 GHz | 1352.1888.13 | |
| Vector network analyzer system, 110 GHz, 4 test ports, complete system based on R&S®ZNA67, 4-port model, standard power | R&S®ZNA67EXT | 10 MHz to 110 GHz | 1352.1888.14 | |
| Vector network analyzer system, 110 GHz, 2 test ports, complete system based on R&S®ZNA67, 2-port model, high power | R&S®ZNA67EXT | 10 MHz to 110 GHz | 1352.1888.0 5 | |
| Vector network analyzer system, 110 GHz, 2 test ports, complete system based on R&S®ZNA67, 4-port model, high power | R&S®ZNA67EXT | 10 MHz to 110 GHz | 1352.1888.16 | |
| Vector network analyzer system, 110 GHz, 4 test ports, complete system based on R&S®ZNA67, 4-port model, high power | R&S®ZNA67EXT | 10 MHz to 110 GHz | 1352.1888.17 | |
| Option | | | | |
| Continuous sweep up to 110 GHz | R&S®ZNA67-K110 | 10 MHz to 110 GHz | 1332.5642.02 | |
| Hardware add-ons | | | | |
| RF cable set, Gore, for R&S®ZNA67EXT, 2-port system | R&S®ZN-ZCASGO | | 1352.1659.02 | |
| RF cable set, Gore, for R&S®ZNA67EXT, 4-port system | R&S®ZN-ZCASGO | | 1352.1659.04 | |

Hardware upgrade options

Hardware options can be retrofitted either with a B option (R&S®ZNA-Bx/-Bxx, R&S®ZNAxx-Bx/-Bxx/-Bxxx) or with a U (upgrade) option. U options are required for the following upgrades:

► Direct source monitor access: R&S®ZNAxx-U161/R&S®ZNAxx-B163.

These options additionally require R&S®ZNAxx-U16 and R&S®ZNAxx-U21/R&S®ZNAxx-U23 unless the corresponding B options (R&S®ZNAxx-B16, R&S®ZNAxx-B21/R&S®ZNAxx-B23) are already installed.

► All source and receiver step attenuators: R&S®ZNAxx-U2n, R&S®ZNAxx-U3n

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